

COMPUTATIONAL STRUCTURAL MECHANICS AND DYNAMICS
Master of Science in Computational Mechanics/Numerical Methods
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Assignment 5:

1. The isoparametric definition of the straight-node bar element in its local system \bar{x} is:

$$\begin{bmatrix} 1 \\ \bar{x} \\ \bar{u} \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 \\ \bar{x}_1 & \bar{x}_2 & \bar{x}_3 \\ \bar{u}_1 & \bar{u}_2 & \bar{u}_3 \end{bmatrix} \begin{bmatrix} N_1^e(\xi) \\ N_2^e(\xi) \\ N_3^e(\xi) \end{bmatrix}$$

Here ξ is the isoparametric coordinate that takes the values -1, 1 and 0 at nodes 1, 2 and 3 respectively, while N_1^e , N_2^e and N_3^e are the shape functions for a bar element. For simplicity, take $\bar{x}_1 = 0$, $\bar{x}_2 = L$, $\bar{x}_3 = \frac{1}{2}L + \alpha L$. Here L is the bar length and α a parameter that characterizes how far node 3 is away from the midpoint location $\bar{x} = \frac{1}{2}L$. Show that the minimum α (minimal in absolute value sense) for which $J = d\bar{x}/d\xi$ vanishes at a point in the element are $\pm \frac{1}{4}$ (the quarter points). Interpret this result as a singularity by showing that the axial strain becomes infinite at an end point.

First of all, the trial functions are defined as the Lagrange interpolation functions of 2nd order:

$$\begin{aligned} N_1^e(\xi) &= \frac{\xi(\xi - 1)}{2} \\ N_2^e(\xi) &= \frac{\xi(\xi + 1)}{2} \\ N_3^e(\xi) &= -(\xi + 1)(\xi - 1) \end{aligned}$$

Using the isoparametric formulation, the geometry mapping is:

$$\bar{x} = \bar{x}_1 N_1^e(\xi) + \bar{x}_2 N_2^e(\xi) + \bar{x}_3 N_3^e(\xi)$$

And the Jacobian is defined as:

$$\begin{aligned} J &= \frac{d\bar{x}}{d\xi} = \bar{x}_1 \frac{dN_1^e(\xi)}{d\xi} + \bar{x}_2 \frac{dN_2^e(\xi)}{d\xi} + \bar{x}_3 \frac{dN_3^e(\xi)}{d\xi} \\ J &= \bar{x}_1 \left(\xi - \frac{1}{2} \right) + \bar{x}_2 \left(\xi + \frac{1}{2} \right) - 2\bar{x}_3 \xi \end{aligned}$$

Substituting the values for the nodal coordinates:

$$J = L \left(\xi + \frac{1}{2} - 2\xi \left(\frac{1}{2} + \alpha \right) \right) = L \left(\frac{1}{2} - 2\alpha\xi \right)$$

The critical value we are searching is when the Jacobian vanishes:

$$0 = L \left(\frac{1}{2} - 2\alpha^* \xi^* \right) \rightarrow \xi^* = \frac{1}{4\alpha^*}$$

The case we are interested is when this critical value fits inside the element domain:

$$-1 \leq \xi^* \leq 1 \rightarrow -1 \leq \frac{1}{4\alpha^*} \leq 1 \rightarrow -\frac{1}{4} \leq \alpha^* \leq \frac{1}{4}$$

In the case that $|\alpha| = \frac{1}{4}$, $\xi^* = \pm 1$. That means that the Jacobian vanishes at one or another end point. In this case, the axial strain become infinite at this point. This is easily shown as:

$$\frac{du}{dx} = \frac{du}{d\xi} \frac{d\xi}{dx} = J^{-1} \frac{du}{d\xi}$$

2. **Extend the result obtained from the previous exercise for a 9-node plane stress element. The element is initially a perfect square, nodes 5, 6, 7, 8 are at the midpoint of the sides 1-2, 2-3, 3-4 and 4-1, respectively, and 9 at the centre of the square. Move node 5 tangentially towards 2 until the Jacobian determinant at 2 vanishes. This result is important in the construction of “singular elements” for fracture mechanics.**

The nodal coordinates are:

$$\begin{aligned} \mathbf{x}_1 &= \begin{bmatrix} -1 \\ -1 \end{bmatrix}, & \mathbf{x}_2 &= \begin{bmatrix} 1 \\ -1 \end{bmatrix}, & \mathbf{x}_3 &= \begin{bmatrix} 1 \\ 1 \end{bmatrix}, & \mathbf{x}_4 &= \begin{bmatrix} -1 \\ 1 \end{bmatrix}, & \mathbf{x}_5 &= \begin{bmatrix} \alpha \\ -1 \end{bmatrix}, \\ \mathbf{x}_6 &= \begin{bmatrix} 1 \\ 0 \end{bmatrix}, & \mathbf{x}_7 &= \begin{bmatrix} 0 \\ 1 \end{bmatrix}, & \mathbf{x}_8 &= \begin{bmatrix} -1 \\ 0 \end{bmatrix}, & \mathbf{x}_9 &= \begin{bmatrix} 0 \\ 0 \end{bmatrix} \end{aligned}$$

The element shape functions are of the Lagrange family:

$$\begin{aligned} N_1^e &= \frac{1}{4}(\xi - 1)(\eta - 1)\xi\eta \\ N_2^e &= \frac{1}{4}(\xi + 1)(\eta - 1)\xi\eta \\ N_3^e &= \frac{1}{4}(\xi + 1)(\eta + 1)\xi\eta \\ N_4^e &= \frac{1}{4}(\xi - 1)(\eta + 1)\xi\eta \\ N_5^e &= \frac{1}{2}(1 - \xi^2)\eta(\eta - 1) \\ N_6^e &= \frac{1}{2}(1 - \eta^2)\xi(\xi + 1) \\ N_7^e &= \frac{1}{2}(1 - \xi^2)\eta(\eta + 1) \\ N_8^e &= \frac{1}{2}(1 - \eta^2)\xi(\xi - 1) \\ N_9^e &= (1 - \xi^2)(1 - \eta^2) \end{aligned}$$

The Jacobian is computed as:

$$J(\xi, \eta) = \sum_{i=1}^9 \begin{bmatrix} x_i \frac{\partial N_i^e}{\partial \xi} & y_i \frac{\partial N_i^e}{\partial \xi} \\ x_i \frac{\partial N_i^e}{\partial \eta} & y_i \frac{\partial N_i^e}{\partial \eta} \end{bmatrix}$$

$$\begin{aligned}
J_{11}(\xi, \eta) = & -\frac{1}{4}(2\xi - 1)(\eta - 1)\eta + \frac{1}{4}(2\xi + 1)(\eta - 1)\eta + \frac{1}{4}(2\xi + 1)(\eta + 1)\eta \\
& - \frac{1}{4}(2\xi - 1)(\eta + 1)\eta - \alpha\xi\eta(\eta - 1) + \frac{1}{2}(1 - \eta^2)(2\xi + 1) \\
& - \frac{1}{2}(1 - \eta^2)(2\xi - 1)
\end{aligned}$$

$$\begin{aligned}
J_{12}(\xi, \eta) = & -\frac{1}{4}(2\xi - 1)(\eta - 1)\eta - \frac{1}{4}(2\xi + 1)(\eta - 1)\eta + \frac{1}{4}(2\xi + 1)(\eta + 1)\eta \\
& + \frac{1}{4}(2\xi - 1)(\eta + 1)\eta + \xi\eta(\eta - 1) - \xi\eta(\eta + 1)
\end{aligned}$$

$$\begin{aligned}
J_{21}(\xi, \eta) = & -\frac{1}{4}(\xi - 1)\xi(2\eta - 1) + \frac{1}{4}(\xi + 1)\xi(2\eta - 1) + \frac{1}{4}(\xi + 1)\xi(2\eta + 1) \\
& - \frac{1}{4}(\xi - 1)\xi(2\eta + 1) + \frac{\alpha}{2}(1 - \xi^2)(2\eta - 1) - \eta\xi(\xi + 1) \\
& + \eta\xi(\xi - 1)
\end{aligned}$$

$$\begin{aligned}
J_{22}(\xi, \eta) = & -\frac{1}{4}(\xi - 1)\xi(2\eta - 1) - \frac{1}{4}(\xi + 1)\xi(2\eta - 1) + \frac{1}{4}(\xi + 1)\xi(2\eta + 1) \\
& + \frac{1}{4}(\xi - 1)\xi(2\eta + 1) - \frac{1}{2}(1 - \xi^2)(2\eta - 1) + \frac{1}{2}(1 - \xi^2)(2\eta + 1)
\end{aligned}$$

Evaluating the Jacobian matrix at the node 2:

$$J(1, -1) = \begin{bmatrix} 1 - 2\alpha & 0 \\ 0 & 1 \end{bmatrix}$$

The determinant is:

$$|J(1, -1)| = 1 - 2\alpha$$

The condition in order the Jacobian to vanish is $\alpha = \frac{1}{2}$. That is, the quarter point.

This condition is the same than in the one dimensional case calculated in the previous case.