







## MASTER OF SCIENCE IN COMPUTATIONAL MECHANICS

### Computational Structural Mechanics and Dynamics

# Assignment 5: Convergence requirements

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### Assignment 5.1 - 1-D Convergence

The isoparametric definition of the straight-node bar element in its local system  $\underline{x}$  is,

$$\begin{bmatrix} 1\\ \bar{x}\\ \bar{u} \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1\\ \bar{x}_1 & \bar{x}_2 & \bar{x}_3\\ \bar{u}_1 & \bar{u}_2 & \bar{u}_3 \end{bmatrix} \begin{bmatrix} N_1^e(\xi)\\ N_2^e(\xi)\\ N_3^e(\xi) \end{bmatrix}$$
(1)

Here  $\xi$  is the isoparametric coordinate that takes the values -1, 1 and 0 at nodes 1, 2 and 3 respectively, while  $N_1^e$ ,  $N_2^e$  and  $N_3^e$  are the shape functions for a bar element.

For simplicity, take  $\bar{x}_1 = 0$ ,  $\bar{x}_2 = l$ ,  $\bar{x}_3 = \frac{1}{2}l + \alpha l$ . Here *l* is the bar length and  $\alpha$  a parameter that characterizes how far node 3 is away from the midpoint location  $\bar{x} = \frac{1}{2}l$ .

Show that the minimum  $\alpha$  (minimal in absolute value sense) for which  $J = d\bar{x}/d\xi$  vanishes at a point in the element are  $\pm \frac{1}{4}$  (the quarter points). Interpret this result as a singularity by showing that the axial strain becomes infinite at an end point.

A geometric representation of the element considered is depicted in Figure (1).



Fig. 1 – Quadratic bar element

For the given element, the shape functions are:

$$N_{1} = \frac{1}{2}\xi(\xi - 1)$$
$$N_{2} = \frac{1}{2}\xi(\xi + 1)$$
$$N_{3} = 1 - \xi^{2}$$

And using expression (1), the geometric coordinate x can be approximated as:

$$x = \bar{x}_1 N_1 + \bar{x}_2 N_2 + \bar{x}_3 N_3$$
  
=  $0 \cdot N_1 + l \cdot \frac{1}{2} \xi(\xi + 1) + (\frac{l}{2} + \alpha l) \cdot (1 - \xi^2)$   
=  $\frac{l}{2} \xi(\xi + 1) + (\frac{l}{2} + \alpha l) \cdot (1 - \xi^2)$ 

Then, the Jacobian can be found as follows:

$$J = \frac{d\bar{x}}{d\xi}$$
  
=  $\frac{l}{2}(\xi + 1) + \frac{l}{2}\xi + (\frac{l}{2} + \alpha l)(-2\xi)$   
=  $l\xi + \frac{l}{2} - l\xi - 2\alpha l\xi$   
=  $\frac{l}{2} - 2\alpha l\xi$ 

which vanishes for  $\alpha = \pm 1/4$  and  $\xi \neq 0$ , i.e. at the end nodes. Moreover, using the expression given in equation (1), the displacement vector is defined as:

$$u = u_1 N_1 + u_2 N_2 + u_3 N_3$$

Considering that the strain  $\varepsilon$  is defined as  $\varepsilon = \frac{du}{dx}$ , it can be obtained that:

$$\begin{split} \varepsilon &= u_1 \frac{dN_1}{dx} + u_2 \frac{dN_2}{dx} + u_3 \frac{dN_3}{dx} \\ &= u_1 \frac{dN_1}{d\xi} \cdot \frac{d\xi}{dx} + u_2 \frac{dN_2}{d\xi} \cdot \frac{d\xi}{dx} + u_3 \frac{dN_3}{d\xi} \cdot \frac{d\xi}{dx} \end{split}$$

Since  $\frac{d\xi}{dx} = J^{-1}$  and J = 0 for  $\alpha = \pm 1/4$  at the end points, the strain value becomes infinite.

#### Assignment 5.2 - 2-D Convergence

Extend the results obtained from the previous Exercise for a 9-node plane stress element. The element is initially a perfect square, nodes 5,6,7,8 are at the midpoint of the sides 1-2, 2-3, 3-4 and 4-1, respectively, and 9 at the center of the square.

Move node 5 tangentially towards 2 until the Jacobian determinant at 2 vanishes. This result is important in the construction of "singular elements" for fracture mechanics.

A geometric representation of the element considered is depicted in Figure (2).



Fig. 2 – Quadratic bar element

For the given element, the shapes functions can be found using the line-product method:

$$N_{1} = \frac{1}{4}\xi\eta(\xi - 1)(\eta - 1) \qquad N_{2} = \frac{1}{4}\xi\eta(\xi + 1)(\eta - 1)$$

$$N_{3} = \frac{1}{4}\xi\eta(\xi + 1)(\eta + 1) \qquad N_{4} = \frac{1}{4}\xi\eta(\xi - 1)(\eta + 1)$$

$$N_{5} = \frac{1}{2}\eta(1 - \xi^{2})(\eta - 1) \qquad N_{6} = \frac{1}{2}\xi(\xi + 1)(1 - \eta^{2})$$

$$N_{7} = \frac{1}{2}\eta(1 - \xi^{2})(\eta + 1) \qquad N_{8} = \frac{1}{2}\xi(\xi - 1)(1 - \eta^{2})$$

$$N_{9} = (1 - \xi^{2})(1 - \eta^{2})$$

Similar to the 1-D case, the geometric coordinates can be interpolated as:

$$x = \sum_{i=1}^{9} x_i N_i$$
  $y = \sum_{i=1}^{9} y_i N_i$ 

Furthermore, the Jacobian matrix **J** for the given problem is defined by the following expression:

$$\mathbf{J} = \begin{bmatrix} \frac{\partial x}{\partial \xi} & \frac{\partial y}{\partial \xi} \\ \frac{\partial x}{\partial \eta} & \frac{\partial y}{\partial \eta} \end{bmatrix} = \begin{bmatrix} \sum_{i=1}^{9} \frac{\partial N_i}{\partial \xi} x_i & \sum_{i=1}^{9} \frac{\partial N_i}{\partial \xi} y_i \\ \sum_{i=1}^{9} \frac{\partial N_i}{\partial \eta} x_i & \sum_{i=1}^{9} \frac{\partial N_i}{\partial \eta} y_i \end{bmatrix}$$

The partial derivatives of the shape functions have the following form:

$$\begin{split} \frac{\partial N_1}{\partial \xi} &= \frac{1}{4} \eta (2\xi - 1)(\eta - 1) & \frac{\partial N_1}{\partial \eta} = \frac{1}{4} \xi (\xi - 1)(2\eta - 1) \\ \frac{\partial N_2}{\partial \xi} &= \frac{1}{4} \eta (2\xi + 1)(\eta - 1) & \frac{\partial N_2}{\partial \eta} = \frac{1}{4} \xi (\xi + 1)(2\eta - 1) \\ \frac{\partial N_3}{\partial \xi} &= \frac{1}{4} \eta (2\xi + 1)(\eta + 1) & \frac{\partial N_3}{\partial \eta} = \frac{1}{4} \xi (\xi + 1)(2\eta + 1) \\ \frac{\partial N_4}{\partial \xi} &= \frac{1}{4} \eta (2\xi - 1)(\eta + 1) & \frac{\partial N_4}{\partial \eta} = \frac{1}{4} \xi (\xi - 1)(2\eta + 1) \\ \frac{\partial N_5}{\partial \xi} &= -\xi \eta (\eta - 1) & \frac{\partial N_5}{\partial \eta} = \frac{1}{2} (1 - \xi^2)(2\eta - 1) \\ \frac{\partial N_6}{\partial \xi} &= \frac{1}{2} (2\xi + 1)(1 - \eta^2) & \frac{\partial N_6}{\partial \eta} = -\xi \eta (\xi + 1) \\ \frac{\partial N_8}{\partial \xi} &= -\xi \eta (\eta + 1) & \frac{\partial N_7}{\partial \eta} = \frac{1}{2} (1 - \xi^2)(2\eta + 1) \\ \frac{\partial N_8}{\partial \xi} &= \frac{1}{2} (2\xi - 1)(1 - \eta^2) & \frac{\partial N_8}{\partial \eta} = -\xi \eta (\xi - 1) \\ \frac{\partial N_9}{\partial \xi} &= -2\xi (1 - \eta^2) \\ \frac{\partial N_9}{\partial \eta} &= -2\eta (1 - \xi^2) \end{split}$$

Now, the case of a quadrilateral element of side l with node 5 having been moved a distance  $\pm a$  (See Figure (3)) will be considered. Thus, for node 2 of the element ( $\xi = 1, \eta = -1$ ), the Jacobian is equal to:

$$\mathbf{J}(1,-1) = \begin{bmatrix} \frac{l}{2} - 2a & 0\\ 0 & \frac{l}{2} \end{bmatrix}$$



Fig. 3 – Element with offset node 5  $\,$ 

Hence, the determinant of the Jacobian vanishes for the following value of  $\alpha$ :

$$|\mathbf{J}(1,-1)| = 0$$
$$\frac{l^2}{4} - la = 0$$
$$a = \frac{l}{4}$$