## **Computational Structural Mechanics and Dynamics**

Assignment 5

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## Assignment 5.1

The isoperimetric definition of the straight-node bar element in its local system x is

$$\begin{bmatrix} 1\\ \bar{x}\\ \bar{u} \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1\\ \bar{x}_1 & \bar{x}_2 & \bar{x}_3\\ \bar{u}_1 & \bar{u}_2 & \bar{u}_3 \end{bmatrix} \begin{bmatrix} N_1^e(\xi)\\ N_2^e(\xi)\\ N_3^e(\xi) \end{bmatrix}$$

Here  $\xi$  is the isoparametric coordinate that takes the values -1, 1 and 0 at the nodes 1, 2 and 3 respectively, while  $N_1^e$ ,  $N_2^e$  and  $N_3^e$  are the shape functions for a bar element. For simplicity, take  $\overline{x_1} = 0$ ,  $\overline{x_2} = L$  and  $\overline{x_3} = \frac{1}{2}L + \alpha L$ . Here L is the bar length and  $\alpha$  a parameter that characterizes how far node 3 is away from the midpoint location  $\overline{x} = \frac{1}{2L}$ . Show that the minimum  $\alpha$  (minimal in absolute value sense) for which  $J = \frac{d\overline{x}}{d\xi}$  vanishes at a point in the element are  $\pm \frac{1}{4}$  (the quarter points). Interpret this result as a singularity by showing that the axial strain becomes infinity at an end point.

- \* CARTESIAN COORDINATES:  $\overrightarrow{X_1}$   $\overrightarrow{X_3}$   $\overrightarrow{X_2}$   $\overrightarrow{X_1} = 0$   $\overrightarrow{X_2} = L$   $\overrightarrow{X_2} = L$  $\overrightarrow{X_3} = \frac{1}{2}L + \alpha L$
- \* NATURAL COORDINATES:  $\frac{1}{y} = \frac{3}{z}$ (1D QUADRATIC ELEMENT) z = -1 z = 0 z = 1

- The Jacobson, can be defined as  $J = \frac{dx}{d\xi}$ , so that, the  $\overline{x}$ is going to be determined, and the Jacobson is going to be coexculated in order to obtain the x values for which J=0

1. The 
$$\overline{x}$$
 is defined as:  $\overline{X} = X_1 N_1 + X_2 N_2 + X_3 N_3$ 

2. Working with a 1D quadratic element, the shape functions  $N = a + bs + cs^2$  being S, the valueal coordinate of the point. Substituting the Svalues at each point the constants values (a, b, c) are determined in each case, being the shape functions:

$$\begin{cases} N_{1}e = \frac{1}{2} \xi(\xi - 1) \\ N_{2}e = \frac{1}{2} \xi(1 + \xi) \\ N_{3}e = 1 - \xi^{2} \end{cases}$$

3. Introducing in the x definition the 3 shape Functions and the contession coordinates values (\$\$1,\$\$2,\$\$3):

$$\overline{\mathbf{X}} = \left[ \frac{1}{2} \widehat{\mathbf{y}} (\widehat{\mathbf{y}} - 1) \right] \mathbf{O} + \left[ \frac{1}{2} \widehat{\mathbf{y}} (\mathbf{1} + \widehat{\mathbf{y}}) \right] \mathbf{L} + \left[ \mathbf{1} - \widehat{\mathbf{y}}^2 \right] (\frac{1}{2} \mathbf{L} + \alpha \mathbf{L}) =$$
$$= \frac{1}{2} \widehat{\mathbf{y}} (\mathbf{1} + \widehat{\mathbf{y}}) \mathbf{L} + \frac{1}{2} \mathbf{L} (\mathbf{1} - \widehat{\mathbf{y}}^2) + \alpha \mathbf{L} (\mathbf{1} - \widehat{\mathbf{y}}^2)$$

9. Now, the Jacobian can be calculated

$$J = \frac{d\bar{x}}{d\bar{y}} = \left(\frac{1}{2} + \frac{1}{2}2\bar{y}\right)L + \left(-\frac{2\bar{y}}{2}L\right) + \left(-2\bar{y}\alpha L\right)$$
$$= \frac{L}{2} - 2\bar{y}\alpha L$$

5. Applying the condition J=0

$$J=0 \implies 0 = \frac{1}{2} - 2\beta \alpha L$$
$$-2\beta \alpha = -\frac{1}{2} \implies \beta \alpha = \frac{1}{4} \implies \alpha = \frac{1}{4\beta}$$

- As the maximum values, talking in absolut value, that s can have are 1 and -1, introducing them in the previous equation, the minimum values (absolute value) that a can get are:

$$\varsigma = 1 \longrightarrow \alpha = \frac{1}{4}$$

$$\varsigma = -1 \longrightarrow \alpha = \frac{-1}{4}$$

- So it can be conclud that the minimum of for which  $J = \frac{d\bar{x}}{d\bar{y}}$  vanishes are  $\pm \frac{1}{4}$
- This result can be interpreted as a sungularity, by collecting the strain of the end points ( $\beta = -1$  and  $\beta = 1$ ).
  - 1. Working with neithral coordinates, the strain matrix can be writed as:

 $[E] = [B] [J-1] [U], \text{ where } J^{-1} \text{ is the investe of}$ the Jacobian.

$$J = \frac{dx}{dx} - p \quad J^{-1} = \frac{dx}{dx}$$

-It has been shown that, at the end points of the element, the Jacobson vanishes, so that, the areal strain Exx;

$$J \neq J = \frac{dx}{ds} = 0 \quad \Rightarrow \quad J^{-1} = \frac{1}{d} = \frac{1}{ds} = \infty$$

- As for cooculate the strain, the B matter is multiplied by the inverse of the Jacobian, (coolculated as ∞), it can be concluded that the strain will be infinity too,

As 
$$J^{-1} = \infty$$
,  $\mathcal{E} = BJ^{-1}U \longrightarrow \mathcal{E}_{XX} = \infty$ 

## Assignment 5.2

Extend the results obtained from the previous Exercise for a 9-node plane stress element. The element is initially a perfect square, nodes 5, 6, 7 and 8 are at the midpoint of the sides 1-2, 2-3, 3-4 and 4-1 respectively and 9 at the center of the square.

Move node 5 tangentially towards 2 until the Jacobian determinant at 2 vanishes. This result is important in the construction of "singular elements" for fracture mechanics.

- how, a 9-node quadrilateral element is going to be studied, in order to check at which point the Jacobian determinant varishes of point 5 is moved torwards node 2.

- First of all, the element an its dimensions are defined

$$\begin{cases} 4 & 7 & 3 \\ 8 & 0 & 0 \\ 9 & 0 & 0 \\ 9 & 0 & 0 \\ 1 & 5 & 2 \\ \end{cases} \begin{pmatrix} x_1 = 0 \\ y_1 = 0 \\ L = 1 \\ L = 1 \\ 1 & 5 & 2 \\ \end{cases}$$

- The length of the square is equal to one and the origin of the cortesian coordinates is fixed at point 1.

- For this kind of element, the Jacobian is defined as

so that, ratural coordinates are introduced, tixing the origin at part 9, where s=0,  $\eta=0$ , and knowing that any  $s \in [-1, 1]$  and any  $\eta \in [-1, 1]$ 



- Finally, in order to conculate the Jacobian determinant x, y and the shape functions should be defined:

• 
$$X = \sum_{i=1}^{q} N_i(s_i \eta) X_i$$

• 
$$y = \sum_{i=1}^{2} Ni(s_i) y_i$$

e The shape functions Ni, i=1...9 definied for the 9-node quadrilateral element can be obtained using the studied methods. - Using the help of Matlab to solve the problem (code attached below), all the needed elements (x, y), shape functions and Jacobson) are defined in order to check at which point of line 1-2, occupated by rode 5, the 15 ranshes.

- As the determinant IJI is collected at point 2, the natural coordinates  $\beta$ ,  $\eta$  take the values:  $\beta = 1$ .  $\eta = -1$
- For rode 5, the what coordinates (X,y) = (o's, o). The X-coordinate changes getting closer to 1.
- Runing the Matlab code, the determinant 151 takes value zero when point 5 coordinates are (x, y) = (0.75, 0), the quarter point of side 1-2.



- The obtained results, (151=0) tell us that for 2D higher order elements the proper location of the corner rodes (1,2,3,4) is not enough. The no-corner rodes, as node 5, should be placed enough close to their natural coordinates in order to avoid local distorsions. Although, this cases have applications in the constructions of special crack elements for linear fracture mechanics,

## MATLAB CODE

```
syms e
syms n
%Shape functions
N1 = 0.25*(e-1)*(n-1)*e*n;
N2 = 0.25*(1+e)*(n-1)*e*n;
N3 = 0.25*(1+e)*(1+n)*e*n;
N4 = 0.25*(e-1)*(1+n)*e*n;
N5 = 0.5*(1-e^2)*(n^2-n);
N6 = 0.5*(e^{2+e})*(1-n^{2});
N7 = 0.5*(1-e^2)*(n^2+n);
N8 = 0.5*(e^2-e)*(1-n^2);
N9 = (1-e^2)*(1-n^2);
% x & y coordinates
% x5 = 0.75
x = 0*N1+1*N2+1*N3+0*N4+0.75*N5+1*N6+0.5*N7+0*N8+0.5*N9;
y = 0*N1+0*N2+1*N3+1*N4+0*N5+0.5*N6+1*N7+0.5*N8+0.5*N9;
%Jacobian
J = [diff(x,e) diff(y,e)]
    diff(x,n) diff(y,n)];
%Determinant
subs (det(J), [e, n], [1 , -1])
```