

# Computational Structural Mechanics and Dynamics, Assignment 5

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## Assignment 5.1

On "Convergence Requirements":

The isoparametric definitions of the straight-node bar element in its local system  $\bar{x}$  is,

$$\begin{bmatrix} 1 \\ \bar{x} \\ \bar{u} \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 \\ x_1 & x_2 & x_3 \\ u_1 & u_2 & u_3 \end{bmatrix} \begin{bmatrix} N_1^e(\xi) \\ N_2^e(\xi) \\ N_3^e(\xi) \end{bmatrix}$$

Here  $\xi$  is the isoparametric coordinate that takes the values -1, 1, 0 and 0 at nodes 1, 2 and 3 respectively, while  $N_1^e$ ,  $N_2^e$  and  $N_3^e$  are the shape functions for a bar element.

For simplicity, take  $x_1 = 0$ ,  $x_2 = L$ ,  $x_3 = \frac{1}{2}l + \alpha l$ . Here  $l$  is the bar length and  $\alpha$  a parameter that characterizes how far away is node 3 from the midpoint location  $x = \frac{1}{2}l$ .

Show that the minimum  $\alpha$  (minimal in absolute value sense) for which  $J = dx/d\xi$  at a point in the element are  $\pm 1/4$  (the quarter points). Interpret this result as a singularity by showing that the axial strain becomes infinite at an end point.

Approximating the x coordinates as:

$$x(\xi) = x_1 N_1(\xi) + x_2 N_2(\xi) + x_3 N_3(\xi)$$

After substituting the expressions for the shape functions:

$$x(\xi) = \frac{1}{2}(x_1 - 2x_3 + x_2)\xi^2 + \frac{1}{2}(x_2 - x_1)\xi + x_3$$

Therefore, the expression of the Jacobian is:

$$J = \frac{dx}{d\xi} = (x_1 - 2x_3 + x_2)\xi + \frac{1}{2}(x_2 - x_1)$$

After substituting that  $x_1 = 0$  and  $x_2 = L$ :

$$J = (-2\alpha l)\xi + \frac{L}{2}$$

Substituting that the Jacobian is zero, and the maximum value of  $\xi = \pm 1$ , one gets:

$$J = 0 \quad \rightarrow \quad \alpha = \pm \frac{1}{4}$$

The strain is calculated as follows:

$$\begin{aligned} \epsilon &= \frac{du}{dx} = \frac{dN_1}{dx}u_1 + \frac{dN_2}{dx}u_2 + \frac{dN_3}{dx}u_3 = \frac{d\xi}{dx} \left( \frac{dN_1}{d\xi}u_1 + \frac{dN_2}{d\xi}u_2 + \frac{dN_3}{d\xi}u_3 \right) \\ &= \frac{1}{J} \left( \frac{dN_1}{d\xi}u_1 + \frac{dN_2}{d\xi}u_2 + \frac{dN_3}{d\xi}u_3 \right) \end{aligned}$$

Therefore, when  $J = 0$  at the extreme of the bar elements, the strains there will be infinity.

### Assignment 5.2

Extend the results obtained from the previous Exercise for a 9-node plane stress element. The element is initially a perfect square, nodes 5,6,7,8 are at the midpoint of the sides 1-2, 2-3, 3-4 and 4-1, respectively, and 9 at the center of the square.

Move node 5 tangentially towards 2 until the Jacobian determinant at 2 vanishes. This result is important in the construction of “singular elements” for fracture mechanics.

In order to attack this point, a MATLAB script was created (Included at the end of this report). What this script does is the following:

- The expressions of the Shape functions are readily entered (Symbolically):
$$N_1 = (1/4) * (1 - \xi) * (1 - \eta) * \xi * \eta;$$

$$N_2 = -(1/4) * (1 + \xi) * (1 - \eta) * \xi * \eta; \dots$$
- The approximations of the coordinates are loaded(Symbolically):
$$x(\xi, \eta) = x_1 N_1(\xi, \eta) + x_2 N_2(\xi, \eta) + \dots + x_9 N_9(\xi, \eta)$$

$$y(\xi, \eta) = y_1 N_1(\xi, \eta) + y_2 N_2(\xi, \eta) + \dots + y_9 N_9(\xi, \eta)$$
- The derivatives are calculated by MATLAB, and they are saved in the Jacobian.

- The values of the coordinates of the nodes of the reference element are entered ( $x_1, x_2, \dots, x_9, y_1, y_2, \dots, y_9$ ), and the values of the  $\xi$  and  $\eta$  coordinates are substituted for node 2. (1,-1)

- The script returns the expression of the Jacobian wrt  $x_5$ .

$$J = 0 = (1 - 2x_5)$$

From the expression returned by the script, one obtains that if the coordinate  $x$  of the node 5 of the quadrilateral is at 1/2, the Jacobian will be negative. This represents 1/4 of the side of the element, just like in the first point of this report for a bar element. Moreover, the factor  $1/\det(J)$  appears in the "B" Matrix, which will cause problems when  $\det(J) \rightarrow 0$ .

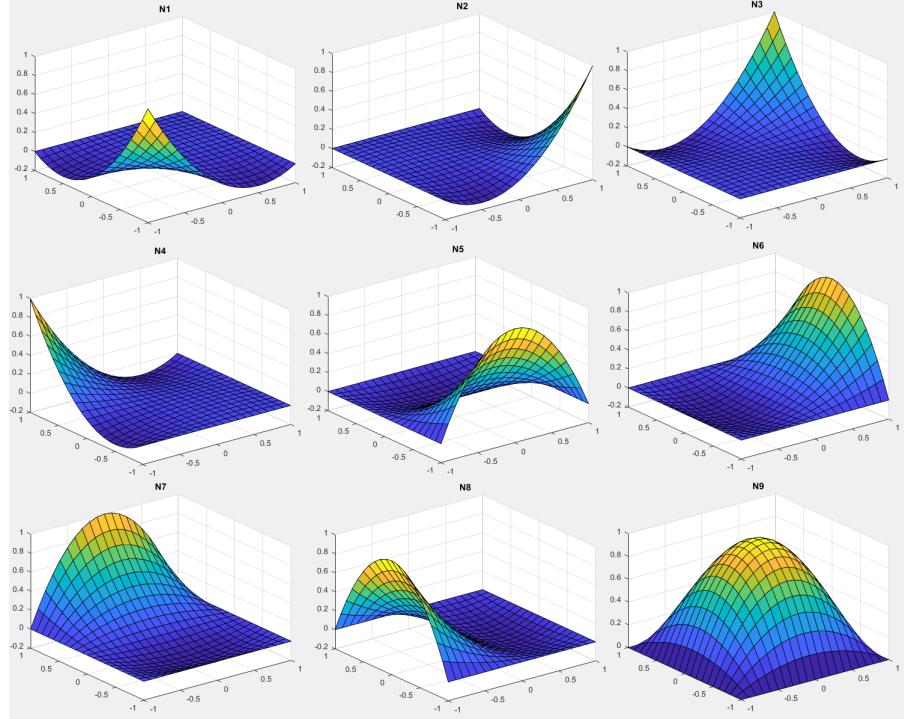


Figure 1: Shape Functions For the 9-Node Quad

## Matlab Code

```

1 %% Script to calculate the determinant of the Jacobian of a 9-
2 %% noded
3 %% Quadrilateral Element
4 %% Jose Raul Bravo Martinez
5 %% MSC Computational Mechanics
6 clear
7 clc
8 close all
9 %%%%%% Plotting the Shape Functions
10 x=[ -1:.1:1];
11 y=[ -1:.1:1];
12
13 [xx,yy]=meshgrid(x,y);
14 N1=xx;
15 for i=1:length(N1)
16     for j=1:length(N1)
17         N1(i,j)=(1/4)*(1- xx(i,j))*(1- yy(i,j))*xx(i,j)*yy(i,j);
18     end
19 end
20 figure(1)
21 surf(xx,yy,N1);
22 title 'N1'
23
24 N2=xx;
25 for i=1:length(N2)
26     for j=1:length(N2)
27         N2(i,j)=-(1/4)*(1+ xx(i,j))*(1- yy(i,j))*xx(i,j)*yy(i,j);
28     end
29 end
30 figure(2)
31 surf(xx,yy,N2);
32 title 'N2'
33
34 N3=xx;
35 for i=1:length(N3)
36     for j=1:length(N3)
37         N3(i,j)=(1/4)*(1+ xx(i,j))*(1+ yy(i,j))*xx(i,j)*yy(i,j);
38     end
39 end
40 figure(3)
41 surf(xx,yy,N3);
42 title 'N3'
43
44 N4=xx;
45 for i=1:length(N4)
46     for j=1:length(N4)
47         N4(i,j)=-(1/4)*(1- xx(i,j))*(1+ yy(i,j))*xx(i,j)*yy(i,j);
48     end
49 end
50 figure(4)
51 surf(xx,yy,N4);
52 title 'N4'
53
54

```

```

55 N5=xx;
56 for i=1:length(N5)
57     for j=1:length(N5)
58         N5(i,j)=-(1/2)*(1 - (xx(i,j)*xx(i,j)))*(1- yy(i,j))*yy(i,j);
59     end
60 end
61 figure(5)
62 surf(xx,yy,N5);
63 title 'N5'

64
65 N6=xx;
66 for i=1:length(N6)
67     for j=1:length(N6)
68         N6(i,j)=(1/2)*(1 + xx(i,j))*(1- (yy(i,j)*yy(i,j)))*xx(i,j);
69     end
70 end
71 figure(6)
72 surf(xx,yy,N6);
73 title 'N6'

74
75 N7=xx;
76 for i=1:length(N7)
77     for j=1:length(N7)
78         N7(i,j)=(1/2)*(1 - (xx(i,j)*xx(i,j)))*(1+ yy(i,j))*yy(i,j);
79     end
80 end
81 figure(7)
82 surf(xx,yy,N7);
83 title 'N7'

84
85
86 N8=xx;
87 for i=1:length(N8)
88     for j=1:length(N8)
89         N8(i,j)=-(1/2)*(1 - xx(i,j))*(1- (yy(i,j)*yy(i,j)))*xx(i,j);
90     end
91 end
92 figure(8)
93 surf(xx,yy,N8);
94 title 'N8'

95
96
97 N9=xx;
98 for i=1:length(N9)
99     for j=1:length(N9)
100        N9(i,j)=(1-xx(i,j)*xx(i,j))*(1-yy(i,j)*yy(i,j));
101    end
102 end
103 figure(9)
104 surf(xx,yy,N9);
105 title 'N9'

106
107
108 %
109 %% Calculating the Determinant
110 %% Calculating the Determinant

```

```

111
112
113
114 syms xi eta X1 X2 X3 X4 X5 X6 X7 X8 X9 Y1 Y2 Y3 Y4 Y5 Y6 Y7 Y8 Y9
115 N1=(1/4)*(1-xi)*(1-eta)*xi*eta;
116 N2=-(1/4)*(1+xi)*(1-eta)*xi*eta;
117 N3=(1/4)*(1+xi)*(1+eta)*xi*eta;
118 N4=-(1/4)*(1-xi)*(1+eta)*xi*eta;
119 N5=-(1/2)*(1-xi^2)*(1-eta)*eta;
120 N6=(1/2)*(1+xi)*(1-eta^2)*xi;
121 N7=(1/2)*(1-xi^2)*(1+eta)*eta;
122 N8=-(1/2)*(1-xi)*(1-eta^2)*xi;
123 N9=(1-xi^2)*(1-eta^2);

124
125 Vect_X=N1*X1+N2*X2+N3*X3+N4*X4+N5*X5+N6*X6+N7*X7+N8*X8+N9*X9;
126 Vect_Y=N1*Y1+N2*Y2+N3*Y3+N4*Y4+N5*Y5+N6*Y6+N7*Y7+N8*Y8+N9*Y9;

127
128
129 J_11= diff(Vect_X ,xi);
130 J_12= diff(Vect_Y ,xi);
131 J_21= diff(Vect_X ,eta);
132 J_22= diff(Vect_Y ,eta);

133
134 Det_J=J_11*J_22-J_21*J_12

135
136 %% Substitute the Value Where you want to calculate the
137 %% determinant [-1,1]^2 %%
138 xi=1; eta=-1;
139 %
140 %
141
142 subs(Det_J)
143 X1=-1;X2=1;X3=-1;X4=-1;X6=1;X7=0;X8=-1;X9=0;Y1=-1;Y2=-1;Y3=1;Y4=1;
144 Y5=-1;Y6=0;Y7=1;Y8=0;Y9=0;
144 subs(Det_J)

```