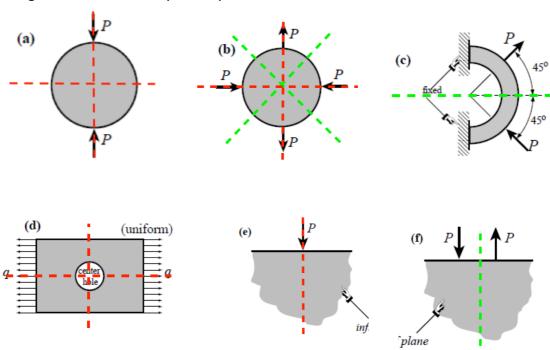
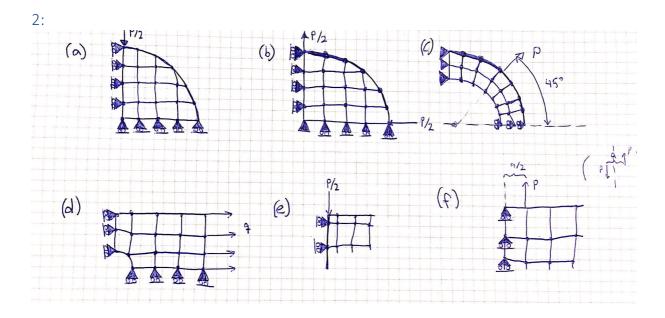
# As2-Benjaminsson

## 2.1

#### 1:

Below the symmetry and anti symmetri lines are shown. Antisymmetry lines are presented with green color and the symmetry lines with red color.





#### 2.2

There are two groups of trouble spots in the example that would need a more fine mesh. At point D there is a concentrated load with sharp contact area and at N, I there are concentrated reaction points. At points B,M,J,F there are entrant corners and abrupt thickness changes.

### 2.3

#### Given:

$$l, \rho, \omega$$

$$A = A_i(1 - \xi) + A_j \xi$$

$$q(x) = \rho A \omega^2 x$$

Prismatic case:  $A = A_i = A_i$ 

#### **Solution:**

With the nodal force in the x-direction we have

$$\begin{split} f_{ext} &= \int_{0}^{1} q \begin{bmatrix} 1 - \xi \\ \xi \end{bmatrix} l d\xi = \int_{0}^{1} \rho \left[ A_{i} (1 - \xi) + A_{j} \xi \right] \omega^{2} x \begin{bmatrix} 1 - \xi \\ \xi \end{bmatrix} l d\xi = \left\{ x_{1} = 0 \to \xi = \frac{x}{l} \right\} = \\ &= \int_{0}^{1} \rho \left[ A_{i} (1 - \xi) + A_{j} \xi \right] \omega^{2} \xi \begin{bmatrix} 1 - \xi \\ \xi \end{bmatrix} l^{2} d\xi = \\ &= \rho l^{2} \omega^{2} \int_{0}^{1} A_{i} \left( \begin{bmatrix} \xi - \xi^{2} \\ \xi^{2} \end{bmatrix} - \begin{bmatrix} \xi^{2} - \xi^{3} \\ \xi^{3} \end{bmatrix} \right) + A_{j} \begin{bmatrix} \xi^{2} - \xi^{3} \\ \xi^{3} \end{bmatrix} d\xi = \\ &= \rho l^{2} \omega^{2} \left[ A_{i} \left( \begin{bmatrix} \frac{\xi^{2}}{2} - \frac{\xi^{3}}{3} \\ \frac{\xi^{3}}{3} \end{bmatrix} - \begin{bmatrix} \frac{\xi^{3}}{3} - \frac{\xi^{4}}{4} \\ \frac{\xi^{4}}{4} \end{bmatrix} \right) + A_{j} \begin{bmatrix} \frac{\xi^{3}}{3} - \frac{\xi^{4}}{4} \\ \frac{\xi^{4}}{4} \end{bmatrix} \right]_{0}^{1} = \\ &= \rho l^{2} \omega^{2} \left[ A_{i} \left( \begin{bmatrix} \frac{1}{2} - \frac{1}{3} \\ \frac{1}{3} \end{bmatrix} - \begin{bmatrix} \frac{1}{3} - \frac{1}{4} \\ \frac{1}{4} \end{bmatrix} \right) + A_{j} \begin{bmatrix} \frac{1}{3} - \frac{1}{4} \\ \frac{1}{4} \end{bmatrix} \right] = \\ &= \rho l^{2} \omega^{2} \left[ A_{i} \left( \frac{1}{12} - \frac{1}{3} \right) + A_{j} \left( \frac{1}{12} - \frac{1}{4} \right) \right]_{0}^{1} = \\ &= \rho l^{2} \omega^{2} \left[ A_{i} \left( \frac{1}{12} - \frac{1}{3} - \frac{1}{4} \right) + A_{j} \left( \frac{1}{12} - \frac{1}{4} \right) \right]_{0}^{1} = \\ &= \rho l^{2} \omega^{2} \left[ A_{i} \left( \frac{1}{12} - \frac{1}{3} - \frac{1}{4} \right) + A_{j} \left( \frac{1}{12} - \frac{1}{4} \right) \right]_{0}^{1} = \\ &= \rho l^{2} \omega^{2} \left[ A_{i} \left( \frac{1}{12} - \frac{1}{3} - \frac{1}{4} \right) + A_{j} \left( \frac{1}{12} - \frac{1}{4} \right) \right]_{0}^{1} = \\ &= \rho l^{2} \omega^{2} \left[ A_{i} \left( \frac{1}{12} - \frac{1}{3} - \frac{1}{4} \right) + A_{j} \left( \frac{1}{12} - \frac{1}{4} \right) \right]_{0}^{1} = \\ &= \rho l^{2} \omega^{2} \left[ A_{i} \left( \frac{1}{12} - \frac{1}{3} - \frac{1}{4} \right) + A_{j} \left( \frac{1}{12} - \frac{1}{4} \right) \right]_{0}^{1} = \\ &= \rho l^{2} \omega^{2} \left[ A_{i} \left( \frac{1}{12} - \frac{1}{3} - \frac{1}{4} \right) + A_{j} \left( \frac{1}{12} - \frac{1}{4} \right) \right]_{0}^{1} = \\ &= \rho l^{2} \omega^{2} \left[ A_{i} \left( \frac{1}{12} - \frac{1}{3} - \frac{1}{4} \right) \right]_{0}^{1} = \\ &= \rho l^{2} \omega^{2} \left[ A_{i} \left( \frac{1}{12} - \frac{1}{3} \right) + A_{j} \left( \frac{1}{12} - \frac{1}{4} \right) \right]_{0}^{1} = \\ &= \rho l^{2} \omega^{2} \left[ A_{i} \left( \frac{1}{12} - \frac{1}{12} - \frac{1}{12} \right) \right]_{0}^{1} = \\ &= \rho l^{2} \omega^{2} \left[ A_{i} \left( \frac{1}{12} - \frac{1}{12} - \frac{1}{12} \right) \right]_{0}^{1} = \\ &= \rho l^{2} \omega^{2} \left[ A_{i} \left( \frac{1}{12} - \frac{1}{12} - \frac{1}{12} \right) \right]_{0}^{1} = \\ &= \rho l^{2} \omega^{2} \left[ A_{i} \left( \frac{1}{12} - \frac{1}{12} - \frac{1}{12} - \frac{1}{12} \right) \right]_{0}^{1} = \\ &= \rho l^{2} \omega^{2} \left[ A_{i} \left( \frac{1}{12} - \frac{1}{12} - \frac{1}{12} - \frac{1}{12} \right) \right]_{0}^{1} = \\ &= \rho l^{2$$

For a prismatic bar with  $A=A_i=A_j$  the consistent nodal force vector becomes

$$f_{ext} = \rho l^2 \omega^2 A \begin{bmatrix} 1/6 \\ 1/3 \end{bmatrix}.$$