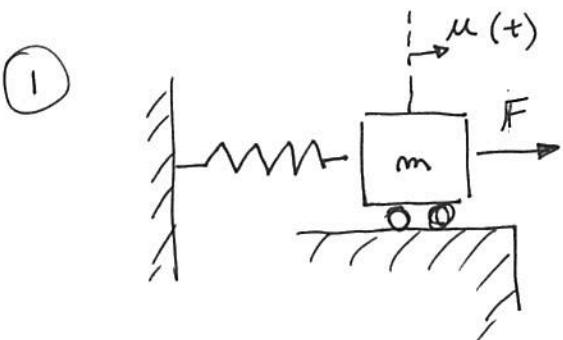


DYNAMICS

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Given the mass m subject to the force F (constant). Describe the effect of F on $u(t)$ [displacement relative to equilibrium] and the natural vibration frequency.

Solution

Using Newton's second law, the sum of forces

is equal to the acceleration of the body.

$$\sum F_{\text{ext}} = m \ddot{u} = m \frac{d^2u}{dt^2} \quad (1)$$

$$\sum F_{\text{ext}} = -ku + F \quad (2)$$

from (1) and (2) it follows that

$$-ku + F = m \frac{d^2u}{dt^2}$$

$$\text{or } \frac{d^2u}{dt^2} + \frac{k}{m} u + \frac{F}{m} = 0 \quad (3)$$

which is a second order O.D.E.
the solution is given by a particular solution and the null space of the equation [solution to the homogeneous equation]

(2)

- using the solution (for the null space)

$$u = A \cos(\omega t + \phi) + B \sin(\omega t + \phi)$$

using $u(0) = 0$, $\phi = 0$ we get

$$\begin{aligned} \frac{d^2 u}{dt^2} &= -A\omega^2 \cos(\omega t + \phi) - B\omega^2 \sin(\omega t + \phi) \\ &= -A\omega^2 \cos(\omega t) - B\omega^2 \sin(\omega t) \quad (4) \end{aligned}$$

Substitute into (3) and we obtain [with $F=0$]

$$-\omega^2 [A \cos(\omega t) + B \sin(\omega t)] + \frac{k}{m} [A \cos(\omega t) + B \sin(\omega t)] = 0$$

since $u(0) = 0$ $A = 0$ (otherwise $u \neq 0$ for $t=0$)

$$\Rightarrow u(t) = B \sin(\omega t); \quad \omega = \sqrt{\frac{k}{m}}$$

(we could have chosen $\phi \neq 0$ and the solution would be different)

- a particular solution is given by

$$u_p = \frac{F}{k} \quad \text{as} \quad u' = u'' = 0$$

$$\text{so (3) becomes } \frac{k}{m} \left(\frac{F}{k} \right) + \frac{F}{m} = 0$$

which is true.

Therefore, the general solution is

$$u(t) = u_p + u_g = \frac{F}{k} + B \sin(\omega t) \quad (5)$$

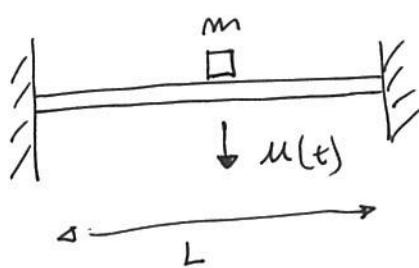
(3)

$$\text{since } \ddot{x} = -\frac{F}{k}$$

$$m = \frac{F}{k} [1 - \sin(\sqrt{\frac{k}{m}} t)] \quad (6)$$

the force F does not affect the natural frequency of the system, only its amplitude.

(2)



Neglecting the mass of the bar, find the natural frequency in terms of m , L , E (of the bar) and A (of the bar).

Solution

Since the system has 1 degree of freedom (vertical displacement of m) we can analyze it as a vertical oscillator. The displacement in the middle of the beam

is

$$m = \frac{FL^3}{16EA^2} = \frac{mgL^3}{16EA^2} \quad (1) \quad (\text{where } F = mg)$$

Balancing forces assuming the force exerted by the bar is linear with the displacement u then $Ku = mg$

$$K \frac{mgL^3}{16EA^2} = mg$$

$$K = \frac{16EA^2}{L^3} \quad (2)$$

(4)

the frequency of vibration is then given by:

$$\omega = \sqrt{\frac{K}{m}} = \sqrt{\frac{16EA^2}{m L^3}} = \frac{4A}{L} \sqrt{\frac{\bar{\epsilon}}{m L^2}} \quad (3)$$

- ③ Use the expression $m = \int \bar{N}^T \bar{N} \rho dV$ (1)
to derive the mass matrix

$$m = \frac{\rho AL}{6} \begin{bmatrix} 1 & 2 \\ 2 & 1 \end{bmatrix} \quad (2)$$

Using the same shape function to derive the stiffness matrix, we obtain a consistent matrix. For a z-modeled bar with 1 D.O.F. (x) the shape functions are

$$N_1 = 1 - \epsilon \quad \text{and} \quad N_2 = \epsilon \quad (3)$$

$$\bar{N} = \begin{bmatrix} N_1 \\ N_2 \end{bmatrix} \quad \bar{N}^T = [N_1 \ N_2]$$

$$\bar{N}^T \bar{N} = [N_1 \ N_2] \begin{bmatrix} N_1 \\ N_2 \end{bmatrix} = \begin{bmatrix} N_1^2 & N_1 N_2 \\ N_1 N_2 & N_2^2 \end{bmatrix} \quad (\text{outer product})$$

$$\Rightarrow m = \frac{\rho A}{L^2} \int_0^L \begin{bmatrix} (L-x)^2 & x(L-x) \\ x(L-x) & x^2 \end{bmatrix} dx \quad (4) \quad dx = L d\epsilon$$

$$m = \frac{\rho AL}{6} \begin{bmatrix} 1 & 2 \\ 2 & 1 \end{bmatrix}$$

(5)

$$\text{Since } \int_0^L (L-x)^2 dx = \int_0^L L^2 - 2Lx - x^2 dx$$

$$= L^3 - \frac{2}{2} L^3 + \frac{L^3}{3} = \frac{L^3}{3}$$

$$\text{and } \int_0^L x(L-x) dx = \int_0^L xL - x^2 dx$$

$$= \frac{L^3}{2} - \frac{L^3}{3} = \frac{3-1}{6} L^3 = \frac{1}{6} L^3$$

- ④ Obtain the mass matrix of a two
noded element with variable x-sectional
area (linearly varying from A_1 to A_2)

$$A(x) = A_1 N_1(x) + A_2 N_2(x) \quad (1)$$

the mass matrix will be given by

$$m = \frac{\rho}{L^2} \int_0^L \begin{bmatrix} (L-x)^2 & x(L-x) \\ x(L-x) & x^2 \end{bmatrix} A(x) dx \quad (2)$$

$$= \frac{\rho}{L^2} \left[A_1 \int_0^L \begin{bmatrix} (L-x)^2 & x(L-x) \\ x(L-x) & x^2 \end{bmatrix} (L-x) dx \right. \\ \left. + A_2 \int_0^1 \begin{bmatrix} (L-x)^2 & x(L-x) \\ x(L-x) & x^2 \end{bmatrix} x dx \right]$$

$$= \frac{\rho}{L^2} \left[A_1 \begin{bmatrix} \frac{L^3}{3} & \frac{L^2}{12} \\ \frac{L^3}{12} & \frac{L^3}{3} \end{bmatrix} + A_2 \begin{bmatrix} \frac{L^3}{12} & \frac{L^3}{12} \\ \frac{L^3}{12} & \frac{L^3}{3} \end{bmatrix} \right]$$

$$= \frac{\rho L}{12} \begin{bmatrix} 3A_1 + A_2 & A_1 + A_2 \\ A_1 + A_2 & A_1 + 3A_2 \end{bmatrix}$$

in the case when $A_1 = A_2$ we obtain
the mass matrix of exercise ③

⑥

- ⑤ A two nodded bar element in 3D has only translational D.O.F. Find the diagonal mass matrix of the element.

Solution:

the bar element will have 6 translational D.O.F.s (3 per mode in each direction, two modes) the mass matrix will only have diagonal terms because the D.O.F.s are only translational. therefore

$$m = \frac{\rho AL}{2} \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}$$

Symm.