## ASSINGMENT 1 COMPUTATIONAL SOLID MECHANICS

## PART1 (rate dependant models)

Rate independent+plain strain assumption
a)

## 1."NON symmetric tension-compression damage"

This implies changing MDtype=3 in main_no interactive.
Next is changing the damage surface in dibujar_criterio_dano1.
Now the surface is $\mathrm{q}=$ stress norm $={ }^{\tau_{\sigma}=\left[\theta+\frac{1-\theta}{n}\right] \sqrt{\sigma: \mathbb{C}^{-1}: \sigma}}$, where n defined in main function ( $\mathrm{n}=3$ ) and tetha depending on main stresses.

$$
\theta=\frac{\sum_{1}^{3}\left\langle\sigma_{i}\right\rangle}{\sum_{1}^{3}\left|\sigma_{\|}\right|}=\frac{\sum_{i}^{3}\left\langle\overline{\sigma_{1}}\right\rangle}{\sum_{1}^{3}\left|\sigma_{i}\right|}
$$

This theta depends on McAuley and absolute value of main stresses, which can be divided in 4 ranges, for each of the quadrants.

For plotting we use the " $\boldsymbol{\sigma}_{1}=r \boldsymbol{\theta} \cos \boldsymbol{\theta} \& \boldsymbol{\sigma}_{1}=\mathrm{r}(\boldsymbol{\theta}) \cos (\boldsymbol{\theta})$ polar coordinates. (radius depending on $\boldsymbol{\theta}$ is the key) and vector "s1" and "s2" sum include point son first and third quadrant. Lines on second and fourth quadrant are just made joining to points attached.


For calculating the stresses must be done on modelos_de_dano1, Tangent constitutive operator $\checkmark$, which is considered constant and given by $\boldsymbol{v}$ and $\mathbf{E}$.

Quadrant $1 \boldsymbol{\sigma}_{1}>0 ; \boldsymbol{\sigma}_{2}>0 ; \boldsymbol{\theta}_{1}=1$
Quadrant $2 \boldsymbol{\sigma}_{1}>0 ; \boldsymbol{\sigma}_{2}<0 ; \boldsymbol{\theta}_{2}=\boldsymbol{\sigma}_{1} /\left(\boldsymbol{\sigma}_{1}+\boldsymbol{\sigma}_{2}\right)$
Quadrant $3 \boldsymbol{\sigma}_{1}<0 ; \boldsymbol{\sigma}_{2}<0 ; \boldsymbol{\theta}_{3}=0$
Quadrant $4 \boldsymbol{\sigma}_{1}<0 ; \boldsymbol{\sigma}_{2}>0 ; \boldsymbol{\theta}_{4}=\boldsymbol{\sigma}_{2} /\left(\boldsymbol{\sigma}_{1}+\boldsymbol{\sigma}_{2}\right)$
we define non-symmetric factor as $\mathrm{F}=(\boldsymbol{\theta}+(1-\boldsymbol{\theta}) / \mathrm{n})$.
Quadrant $1 \boldsymbol{\theta}_{1}=1 ; F=1$
Quadrant $2 \boldsymbol{\theta}_{2}=\boldsymbol{\sigma}_{1} /\left(\boldsymbol{\sigma}_{1}+\boldsymbol{\sigma}_{2}\right)=\cos \boldsymbol{\theta} /(\cos \boldsymbol{\theta}+\sin \boldsymbol{\theta}) ; \mathrm{F}=\left(\boldsymbol{\theta}_{2}+\left(1-\boldsymbol{\theta}_{2}\right) / \mathrm{n}\right)$
Quadrant3 $\boldsymbol{\theta}_{3}=0$;
Quadrant $4 \boldsymbol{\theta}_{4}=\boldsymbol{\sigma}_{2} /\left(\boldsymbol{\sigma}_{1}+\boldsymbol{\sigma}_{2}\right)=\sin \boldsymbol{\theta} /(\cos \boldsymbol{\theta}+\sin \boldsymbol{\theta}) ; \mathrm{F}=\left(\boldsymbol{\theta}_{2}+\left(1-\boldsymbol{\theta}_{4}\right) / \mathrm{n}\right)$
Strain norm will be same as symmetric case, divided by this factor, which depends on main stresses.

## 2."Tensile-only" damage model

Plotting is quite trivial, just taking profit of first quadrant and plotting two straight lines. This must be done at dibujar_criterio_dano1.


Again, for calculating the stresses must be done on modelos_de_dano1, Tangent constitutive operator $\mathbb{\checkmark}$, which is considered constant and given by $\boldsymbol{v}$ and $\mathbf{E}$.

## 3d quadrant

We assume Strain norm $=0$ for other quadrants than the first one.
b)

## Implement linear and exponential hardening/softening ( $\mathrm{H}<0, \mathrm{H}>0$ )

## Linear

Linear is already implemented. To implement exponential will be necessary to modify rmap_dano1, which calculates the stress path depending on hardening function assumption.

Only loading variant will take into account the hardening function.
It's remarkable that of $\mathrm{H}<0$, the elastic domain diminishes, and if it's $\mathrm{H}>0$ it increases (e.g. metal cases). In this last case the damage leds to a more resistance a posterior stress.

## Exponential

when:
$\mathrm{q}_{\text {inf }}<\mathrm{r}_{0}-->$ elastic domain diminishes
$q_{\text {inf }}>r_{0}$, it increases.
$\mathrm{q}_{\text {inf }}=\mathrm{r}_{0}$ Elastic domain remains the same
it's been detected that when it $\mathrm{q}_{\text {inf }}>\mathrm{r}_{0}$, "A" takes an important role in correct behaviour of simulation.
Hypothesis: It has to be taken into account that aux_var(6) $=q_{n+1} / r_{n+1}$ has to be bigger than $\mathrm{q}_{\mathrm{n}} / r_{\mathrm{n}}$ in order to damage never decrease.

With $\mathrm{q}_{\text {inf }}=2$ and $\mathrm{A}=2$ :

## Examples on 4 combinations:

Exponential symmetric case


Linear symmetric


Non sym exponential



Both cases, more damage in linear, though elastic domain does increases in exponential vs linear.
c)

## For each case obtain stress space and stress strain

Considering EXPONENTIAL HARDENING/SOFTENING in order to linear/non linear behaviour to be more obvious.

1. $\Delta \sigma_{1}{ }^{(1)}=\alpha ; \Delta \sigma_{2}{ }^{(1)}=0$
$\Delta \boldsymbol{\sigma}_{1}{ }^{(2)}=-\beta ; \Delta \boldsymbol{\sigma}_{2}{ }^{(2)}=0$
$\Delta \boldsymbol{\sigma}_{1}{ }^{(3)}=\gamma ; \Delta \boldsymbol{\sigma}_{3}{ }^{(3)}=0$

SIGMAP $=(\alpha 0, \alpha-\beta 0, \alpha-\beta+\gamma 0)$

Symmetric


First path 1-11
1 to 5 Elastic domain. No damage. Linear behaviour. REACHES damage surface.
5 to 11 Load. Damage. Damage Surface increases.
First path 11-21
11 to 21 Unload. No damage. Elastic behaviour $\left(E_{d}\right)$
First path 21-31
21-27 Elastic domain. No damage. Linear behaviour. REACHES damage surface. 27 to 31 Load. Damage Surface (already increased) increases more. reaches at $\sigma_{2}=284$ vs $\sigma_{2}=200$ of point 5.

- Non Symmetric tension-compression: Same
- tension-only case:Same

2. $\Delta \boldsymbol{\sigma}_{1}{ }^{(1)}=\alpha ; \Delta \sigma_{2}{ }^{(1)}=0$
$\Delta \boldsymbol{\sigma}_{1}{ }^{(2)}=-\beta ; \Delta \boldsymbol{\sigma}_{2}{ }^{(2)}=-\beta$
$\Delta \boldsymbol{\sigma}_{1}{ }^{(3)}=\gamma ; \Delta \sigma_{3}{ }^{(3)}=\gamma$
$\operatorname{SIGMAP}=(\alpha 0, \alpha-\beta-\beta, \alpha-\beta+\gamma-\beta+\gamma)$
Symmetric


## First path 1-11

1 to 8 Elastic domain. No damage. Linear behaviour. REACHES damage surface. 8 to 11 Load. Damage. Damage Surface increases.

First path 11-21
11 to 21 Unload. No damage. Elastic behaviour $\left(E_{d}\right)$

## First path 21-31

21-25 Elastic domain. No damage. Linear behaviour. REACHES damage surface. 25 to 31 Load. Damage Surface (already increased) increases more.

Non Symmetric tension-compression


Very similar to symmetric case:
First path 1-11
1 to 8 Elastic domain. No damage. Linear behaviour. REACHES damage surface.
8 to 11 Load. Damage. Damage Surface increases.
First path 11-21
11to 21 Unload. No damage. Elastic behaviour $\left(E_{d}\right)$

First path 21-31
21-26 Elastic domain. No damage. Linear behaviour. REACHES damage surface. 26 to 31 Load. Damage Surface (already increased) increases more. Reaches surface at $\sigma_{2}=287$ vs $\sigma_{2}=158$ of point 26.

Tension-only case


First path 1-11
1 to 8 Elastic domain. No damage. Linear behaviour. REACHES damage surface.
8 to 11 Load. Damage. Damage Surface increases.
First path 11-21
11 to 21 Unload. No damage. Elastic behaviour ( $\mathrm{E}_{\mathrm{d}}$ )
First path 21-31
21-26 Elastic domain. No damage. Linear behaviour. REACHES damage surface. 26 to 31 Load. Damage Surface (already increased) increases more. Reaches surface at $\sigma_{2}=288$ vs $\sigma_{2}=210$ of point 19-20.
3. $\quad \Delta \sigma_{1}{ }^{(1)}=\alpha ; \Delta \sigma_{2}{ }_{2}^{(1)}=\alpha$
$\Delta \boldsymbol{\sigma}_{1}{ }^{(2)}=-\beta ; \Delta \sigma_{2}{ }^{(2)}=-\beta$
$\Delta \sigma_{1}{ }^{(3)}=\gamma ; \Delta \sigma_{3}{ }^{(3)}=\gamma$
SIGMAP $=(\alpha \alpha, \alpha-\beta \alpha-\beta, \alpha-\beta+\gamma \alpha-\beta+\gamma)$

## Symmetric



First path 1-11
1 to 7 Elastic domain. No damage. Linear behaviour. REACHES damage surface.
7 to 11 Load. Damage. Damage Surface increases.

## First path 11-21

11 to 21 Unload. No damage. Elastic behaviour ( $E_{d}$ )
First path 21-31
21-22 Elastic domain. No damage. Linear behaviour. REACHES damage surface. 22 to 31 Load. Damage Surface (already increased) increases more.

- Non Symmetric tension-compression: Same
- tension-only case:Same

ANEXO 1

```
function [rtrial] = Modelos_de_dano1 (MDtype,ce,eps_n1,n)
if (MDtype==1) %* Symmetric
    rtrial= sqrt(eps_n1*ce*eps_n1');
    elseif (MDtype==2) %* Only tension
sigma=ce*eps_n1';
sigma1=sigma(1);
sigma2=sigma(2);
if (sigma1>0)&&(sigma2>0)
rtrial= sqrt(eps_n1*ce*eps_n1')
elseif (sigma1<0)&&(sigma2<0)
rtrial=0;
elseif ((sigma1<0)&&(sigma2>0)) %!!!!
    rtrial=0;
elseif ((sigma1>0)&&(sigma2<0)) %!!!!
        rtrial=0;
end
    elseif (MDtype==3) %*Non-symmetric
sigma=ce*eps_n1';
sigma1=sigma(1);
sigma2=sigma(2);
if (sigma1>0)&&(sigma2>0)
rtrial= sqrt(eps_n1*ce*eps_n1')
elseif (sigma1<0)&&(sigma2<0)
rtrial= sqrt(eps_n1*ce*eps_n1')*n;
elseif ((sigma1<0)&&(sigma2>0))
    tetha=sigma2/(sigma1+sigma2);
    F=tetha+(1-tetha)/n;
    rtrial= sqrt(eps_n1*ce*eps_n1')/F;
elseif ((sigma1>0)&&(sigma2<0)) %%%%%%%aqui!!!!!!!!
    tetha=sigma1/(sigma1+sigma2);
    F=tetha+(1-tetha)/n;
    rtrial= sqrt(eps_n1*ce*eps_n1')/F;
end
end
```

return

```
function plotcurvesNEW(DATA,vpx,vpy,LABELPLOT,vartoplot)
% Plot stress vs strain (callback function)
% ------------------------------------------
```


\% PLOTTING
ncolores $=3$;
colores $=$ ColoresMatrix(ncolores);
markers = MarkerMatrix(ncolores) ;
subplot $(2,2,3)$
title('DAMAGE')
hold on
grid on
xlabel (vpx)
ylabel(vpy)
switch vpx
case 'STRAIN_1'
strx $=$ 'X(i) = DATA.strain(i,1);' ;
\%strx $=$ 'X(i) $=\max (D A T A . s t r a i n(i, 1), D A T A . s t r a i n(i, 2)) ; ' ;$
case 'STRAIN_2'
strx $=$ 'X(i) = DATA.strain(i,2);' ;
\%strx $=$ 'X(i) $=$ min(DATA.strain(i,1),DATA.strain(i,2));' ;
case '|STRAIN_1|'
strx $=$ 'X(i) = abs(DATA.strain(i,1));' ;
\%strx = 'X(i) = abs (max(DATA.strain(i,1), DATA.strain(i,2)));' ;
case '|STRAIN 2|'
strx $=$ 'X(i) = abs(DATA.strain(i,2));' ;
\%strx $=$ 'X(i) $=$ abs(min(DATA.strain(i,1),DATA.strain(i,2)));' ;
case 'norm(STRAIN)'
strx $=$ 'X(i) $=\operatorname{sqrt((DATA.strain(i,1))\wedge 2+(DATA.strain(i,2))\wedge 2));';~}$
case 'TIME'
strx $=$ 'X(i) =DATA.TIMEVECTOR(i) ;';
otherwise
for iplot $=1:$ length (LABELPLOT)
switch vpx
case LABELPLOT\{iplot\}
strx = ['X(i) = vartoplot\{i\}(',num2str(iplot),') ;'];
end
end
end
$\mathrm{X}=0$;
for i $=1: s i z e(D A T A . s t r a i n, 1)$
eval(strx) ;
end
\% DATA Y
\% ------
switch vpy

```
case 'STRESS_1'
    stry = 'Y(i) = DATA.sigma_v{i} (1,1);' ;
    %stry = 'Y(i) = max(DATA.sigma_v{i}(1,1),DATA.sigma_v{i}(2,2));' ;
case 'STRESS_2'
    stry = 'Y(i) = DATA.sigma_v{i} (2,2);' ;
    %stry = 'Y(i) = min(DATA.sigma_v{i}(1,1),DATA.sigma_v{i}(2,2));' ;
case '|STRESS_1|'
    %stry = 'Y(i) = abs(max(DATA.sigma_v{i}(1,1),DATA.sigma_v{i}(2,2)));' ;
    stry = 'Y(i) = abs(DATA.sigma_v{i}(1,1));' ;
case '|STRESS_2|'
    %stry = 'Y(i) = abs(min(DATA.sigma_v{i}(1,1),DATA.sigma_v{i}(2,2)));' ;
    stry = 'Y(i) = abs(DATA.sigma_v{i} (2,2));' ;
case 'norm(STRESS)'
    stry = 'Y(i) = sqrt((DATA.sigma_v{i}(1,1))^2+(DATA.sigma_v{i}(2,2))^2);' ;
case 'DAMAGE VAR.'
    stry = 'Y(i) = sqrt((DATA.sigma_v{i}(1,1))^2+(DATA.sigma_v{i}(2,2))^2);' ;
otherwise
    for iplot = 1:length(LABELPLOT)
            switch vpy
                case LABELPLOT{iplot}
                    stry = ['Y(i) = vartoplot{i}(',num2str(iplot),') ;'];
            end
    end
end
Y = 0;
for i = 1:length(DATA.sigma_v)
    try
        eval(stry);
    end
end
plot(X,Y,'Marker',markers{1},'Color', colores(1,:));
for i=1:length(X)
    text(X(i),Y(i),num2str(i));
end
```

Not enough input arguments.

Error in plotcurvesNEW (line 20)
xlabel(vpx);

```
function strain =PlotIniSurf(YOUNG_M,POISSON,YIELD_STRESS,SIGMAP,ntype,MDtype,n,istep)
%***************************************************************************************
Eprop=[YOUNG_M POISSON O YIELD_STRESS];
sigma_u =YIELD_STRESS ;
E = YOUNG_M ;
nu = POISSON ;
%
%* Evaluar el tensor constitutivo elïi1/2stico (Matriz de Hooke) %*
%* Llamado de Rutina tensor_elasticol %*
[ce] = tensor_elastico1 (Eprop, ntype);
%}***********************************************************************************************
%
%* Dibujo de la superficie de daï ¿1⁄20}\quad%
```



```
figure(1);
set(1,'Name','ANALYSIS OF A DAMAGE MODEL (GAUSS POINT LEVEL)')
hold on;
%dbstop('122')
subplot(1,2,1);
title('Damage surface (principal stresses axes)')
xlabel('\sigma_{1}')
ylabel('\sigma_{2}')
hold on;
grid on;
pbaspect([2 1 1]); %%escala ejes es igual
q=sigma_u/sqrt(E);
hplot = dibujar_criterio_dano1(ce, nu, q , 'b-', MDtype,n );
%%%%%
if ntype == 2
    SIGMAP = [0 0;SIGMAP] ;
    mstrain = 4 ;
    hplotquiver = [] ;
    STRAIN = zeros(size(SIGMAP,1),4);
    for iloc = 1:size(SIGMAP,1)-1
        SSS =SIGMAP(iloc,:);
        sigma_bef=[SSS(1) SSS(2) 0 nu*(SSS(1)+SSS(2))];
        SSS =SIGMAP(iloc+1,:);
        sigma_0=[SSS(1) SSS(2) 0 nu*(SSS(1)+SSS(2))];
        % hplotquiver(end+1) = plot([sigma_bef(1) sigma_0(1)],[sigma_bef(2) sigma_0(2)
]) ;
        plot( sigma_0(1), sigma_0(2),'b*')
        text( sigma_0(1), sigma_0(2),['P=',num2str(iloc)]);
        strain_di =(inv(ce)*sigma_0')';
        STRAIN(iloc+1,:) = strain_di ;
```

```
        end
end
% PLOTTING (PATH)
% ********
% Divide SIGMAP{end} - SIGMAP{end-1} in istep1 steps
hplotp = [];
[ hplotp hplotl]=plotpathNI(SIGMAP,istep);
[strain] = calstrain_NI(istep,STRAIN) ;
```

Not enough input arguments.

Error in PlotIniSurf (line 6)
Eprop=[YOUNG_M POISSON 0 YIELD_STRESS];

```
function [hplotp, hplotl]=plotpathNI(SIGMAP,istep)
% See select_path
% It plots stress path
% Plot iloc-th stretch
% --------------------
PNT = SIGMAP(1,:) ;
hplotp = plot(PNT(1),PNT(2),'ro');
hplotl = [] ;
for iloc = 1:size(SIGMAP,1)-1
    INCSIGMA = SIGMAP(iloc+1,:)-SIGMAP(iloc,:) ;
    for i = 1:istep(iloc)
        PNTb = PNT ;
        % PNT = PNT+INCSIGMA* ;
        PNT = PNT+INCSIGMA/(istep(iloc));
        LINE = [PNTb ; PNT] ;
        hplotp(end+1) = plot(PNT(1) ,PNT(2),'ro');
        hplotl(end+1) = plot(LINE(:,1) ,LINE(:,2),'r','LineWidth',1,'LineStyle','--');
    end
end
```

Not enough input arguments.

Error in plotpathNI (line 7)
$\operatorname{PNT}=\operatorname{SIGMAP}(1,:)$;

```
function [sigma_n1,hvar_n1,aux_var] = rmap_dano1 (eps_n1,hvar_n,Eprop,ce,MDtype,n)
%
%*
    Integration Algorithm for a isotropic damage model
%*
%*
%* [sigma_n1,hvar_n1,aux_var] = rmap_dano1 (eps_n1,hvar_n,Eprop,ce)
% *
%* INPUTS
    hvar_n(6) internal variables , step n
    hvar n(1:4) (empty)
    hvar_n(5) = r ; hvar_n(6)=q
    Eprop(:) Material parameters
    ce(4,4) Constitutive elastic tensor
%* OUTPUTS: sigma_n1(4) Cauchy stress , step n+1
%* hvar_n(6) Internal variables , step n+1
*
%* aux_var(3) Auxiliar variables for computing const. tangent tensor
*
%
```

hvar_n1 = hvar_n;
r_n $=$ hvar_n(5);
q_n $=$ hvar_n(6);
E $\quad=$ Eprop (1);
nu $\quad=$ Eprop (2);
H $\quad=$ Eprop (3) ;
sigma_u = Eprop(4);
hard type $=$ Eprop(5) ;


\%* initializing
r0 = sigma_u/sqrt(E);
zero_q=1.d-6*r0;
\% if(r_n<=0.d0)
\% r_n=r0;
\% $\quad$ _n=r0;
\% end


\% Damage surface $\%$ 五
[rtrial] = Modelos_de_dano1 (MDtype, ce,eps_n1,n);


\%* Ver el Estado de Carga \%
\%* ---------> fload=0 : elastic unload \%*
\%* ---------> fload=1 : damage (compute algorithmic constitutive tensor) \%*
fload=0;

```
if(rtrial > r_n)
    %* Loading
    fload=1;
    delta_r=rtrial-r_n;
    r_n1= rtrial ;
    if hard_type == 0
        % Linear
        q_n1= q_n+ H*delta_r; %remember that H=0,1, wich is >0, thus hardening
    else
        %exponential!!!!!!!!
        A=6; %if A=0; Elastic domain remains the same
        qinf=2; %qinf<0-->elastic domain diminishes, qinf>r0, it increases.
        q_n1=qinf-(qinf-q_n)*exp(A*(1-rtrial/r_n));
    end
    if(q_n1<zero_q)
        q_n1=zero_q;
    end
else
    %* Elastic load/unload
    fload=0;
    r_n1= r_n ;
    q_n1= q_n ;
end
% Damage variable
% ---------------
dano_n1 = 1.d0-(q_n1/r_n1);
% Computing stress
% ****************
sigma_n1 =(1.d0-dano_n1)*ce*eps_n1';
%hold on
%plot(sigma_n1(1),sigma_n1(2),'bx')
%*************************************************************************************
%*************************************************************************************
%* Updating historic variables
                                    %*
% hvar_n1(1:4) = eps_n1p;
hvar_n1(5)= r_n1 ;
hvar_n1 (6) = q_n1 ;
%
%
%* Auxiliar variables %*
aux var(1) = fload;
aux_var(2) = q_n1/r_n1;
%*aux_var(3) = (q_n1-H*r_n1)/r_n1^3;
%**************************************************************************************
```

```
function [ce] = tensor_elastico1 (Eprop, ntype)
%*************************************************************************************
%* Elastic constitutive tensor %*
%
%*************************************************************************************
%
%* G --------> Shear modulus %*
%* K --------> Bulk modulus
    %*
G=Eprop (1)/(2*(1+Eprop (2)));
K=Eprop(1)/(3*(1-2*Eprop (2)));
%******************************************************************************************
if(ntype==1) % Plane stress
elseif(ntype==2) % Plane strain
    ce = zeros(4,4); % Init.
    C1=K+(4.0D0/3.0D0)*G;
    C2=K-(2.0D0/3.0D0) *G;
    ce (1,1) =c1;
    ce (2, 2) =c1;
    ce (4,4)=c1;
    ce (1, 2) = C2;
    ce (1,4) = C2;
    ce (2,4) = C2;
    ce (2,1)=C2;
    ce (4,1)=C2;
    ce (4,2)=C2;
    ce (3,3)=G;
elseif(ntype==4) % Tres Dimensiones
end
%*************************************************************************************
return
```

Not enough input arguments.

Error in tensor_elastico1 (line 11)
G=Eprop (1) / (2*(1+Eprop (2))) ;

## Contents

- Plot Initial Damage Surface and effective stress path

```
clc
clear all
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
% Program for modelling damage model
% (Elemental gauss point level)
% -----------------
% Developed by J.A. Hdez Ortega
% 20-May-2007, Universidad PolitÃ`cnica de CataluÃ\pma
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%profile on
% ------------------------
% ****************
% INPUTS
% ****************
% YOUNG's MODULUS
% ---------------
YOUNG_M = 20000 ;
% Poisson's coefficient
% -----------------------
POISSON = 0.3 ;
% Hardening/softening modulus
% -----------------------------
HARDSOFT_MOD = 0.1 ;
% Yield stress
% ------------
YIELD_STRESS = 200;
% Problem type TP = {'PLANE STRESS','PLANE STRAIN','3D'}
% ------------------------ = 1 =2 =3
%
ntype= 2 ;
% Model PTC = {'SYMMETRIC','TENSION','NON-SYMMETRIC'} ;
% = 1 = 2 = 3
% --------------------------------------------------------
MDtype =1;
% Ratio compression strength / tension strength
% ---------------------------------------------------
n = 3 ;
% SOFTENING/HARDENING TYPE
% -------------------------
HARDTYPE = 'EXP' ; %{LINEAR,EXPONENTIAL} %diferente de linear es suficiente
% VISCOUS/INVISCID
% ------------------------
VISCOUS = 'NO' ;
% Viscous coefficient ----
% --------------------------
eta = 0.3 ;
% TimeTotal (initial = 0) ----
% ------------------------
TimeTotal = 10 ; ;
% Integration coefficient ALPHA
% ------------------------
ALPHA_COEFF = 0.5 ;
% Points
```

```
%
nloadstates = 3 ;
SIGMAP = zeros(nloadstates,2) ;
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
% {
SIGMAP(1,:) = [300 400];
SIGMAP(2,:) =[500 400];
SIGMAP (3,:) = [500 0];
% }
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
Su=YIELD_STRESS;
alfa=[300 150 600];
%%%%%%%%%%%%%%%%%%%%
%tipo de caso del problema c
    num='3';
%%%%%%%%%%%%%%%%%%
switch num
    case 'def'
    SIGMAP(1,:) = [300 400];
    SIGMAP(2,:) = [500 400];
    SIGMAP(3,:) =[500 0];
    case '1'
    SIGMAP(1,:) = [alfa(1) 0];
    SIGMAP (2,:) = [alfa(1)-alfa(2) 0];
    SIGMAP(3,:) = [alfa(1)-alfa(2)+alfa(3) 0];
    case '2'
    SIGMAP(1,:) = [alfa(1) 0];
    SIGMAP(2,:) = [alfa(1)-alfa(2) (-alfa(2))];
    SIGMAP(3,:) = [alfa(1)-alfa(2)+alfa(3) (-alfa(2)+alfa(3))];
    otherwise
    SIGMAP(1,:) = [alfa(1) alfa(1)];
    SIGMAP(2,:) =[alfa(1)-alfa(2) alfa(1)-alfa(2)];
    SIGMAP(3,:) = [alfa(1)-alfa(2)+alfa(3) alfa(1)-alfa(2)+alfa(3)];
end
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
% Number of time increments for each load state
% -----------------------------------------
istep = 10*ones(1,nloadstates) ;
% VARIABLES TO PLOT
vpx = 'TIME' ; % AVAILABLE OPTIONS: 'STRAIN_1', 'STRAIN_2'
% '|STRAIN_1|', '|STRAIN_2|'
% 'norm(STRAIN)', 'TIME'
vpy = 'damage variable (d)' % AVAILABLE OPTIONS: 'STRESS_1', 'STRESS_2'
% '|STRESS_1|', '|STRESS_2|'
% 'norm(STRESS)', 'TIME', 'DAMAGE VAR.','hardening variable (q)','damage variable (d)'
% 'internal variable (r)'
    3) LABELPLOT{ivar} --> Cell array with the label string for
% variables of "varplot"
%
LABELPLOT = {'hardening variable (q)','internal variable (r)','damage variable (d)'};
%%%%%%%%%%%%%%%%%%%%%5 END INPUTS %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
```


## Plot Initial Damage Surface and effective stress path

```
strain_history = PlotIniSurf(YOUNG_M,POISSON,YIELD_STRESS,SIGMAP,ntype,MDtype,n,istep);
E = YOUNG_M ;
nu = POISSON ;
sigma_u = YIELD_STRESS ;
switch HARDTYPE
    case 'LINEAR'
        hard_type = 0 ;
    otherwise
        hard_type = 1 ;
end
switch VISCOUS
    case 'YES'
    viscpr = 1 ;
    otherwise
        viscpr = 0 ;
end
Eprop = [E nu HARDSOFT_MOD sigma_u hard_type viscpr eta ALPHA_COEFF]
% DAMAGE MODEL
% ------------
[sigma_v,vartoplot, LABELPLOT_out,TIMEVECTOR]=damage_main(Eprop,ntype,istep,strain_history,
MDtype,n,TimeTotal);
try; LABELPLOT;catch;LABELPLOT = LABELPLOT_out ; end ;
% PLOTTING
% -------
ncolores = 3 ;
colores = ColoresMatrix(ncolores);
markers = MarkerMatrix(ncolores) ;
hplotLLL = [] ;
for i = 2:length(sigma_v)
    stress_eig = sigma_v{i} ; %eigs(sigma_v{i}) ;
    tstress_eig = sigma_v{i-1}; %eigs(sigma_v{i-1}) ;
    hplotLLL(end+1) = plot([tstress_eig(1,1) stress_eig(1,1) ],[tstress_eig(2,2) stress_ei
g(2, 2)],'LineWidth',2,'color', colores(1, :),'Marker',markers{1},'MarkerSize', 2);
```

```
plot(stress_eig(1,1),stress_eig(2,2),'bx')
text(stress_eig(1,1),stress_eig(2,2),num2str(i))
% SURFACES
% -----
end
SURFACES
% -----
if(aux_var (1)>0)
    hplotSURF(i) = dibujar_criterio_danol(ce, nu, hvar_n(6), 'r:',MDtype,n );
    set(hplotSURF(i),'Color',[0 0 1],'LineWidth',1);
end
```

```
DATA.sigma_v = sigma_v ;
```

DATA.sigma_v = sigma_v ;
DATA.vartoplot = vartoplot ;
DATA.vartoplot = vartoplot ;
DATA.LABELPLOT = LABELPLOT ;
DATA.LABELPLOT = LABELPLOT ;
DATA.TIMEVECTOR = TIMEVECTOR ;
DATA.TIMEVECTOR = TIMEVECTOR ;
DATA.strain = strain_history ;
DATA.strain = strain_history ;
%plotcurvesNEW(DATA,vpx,vpy,LABELPLOT,vartoplot) ;
subplot(1,2,2)
%%%%%%%%%%%%%%%%%%%%%%%%%%%
set(1,'Name','ANALYSIS OF A DAMAGE MODEL (GAUSS POINT LEVEL)')
hold on;
title('STRESS-STRAIN')
xlabel('STRAIN')
ylabel('STRESS')
hold on;
grid on;
%%%%%%%%%
strain11=strain_history(:,1);
stress11=zeros(nloadstates*istep(1)+1,1);
num=zeros(1,nloadstates*istep(1) +1);
for i=1:31
stress11(i)=sigma_v{i}(1,1);
num(i)=i;
end
size(strain11);
size(stress11);
plot(strain11,stress11,'r');

```
```

ncolores = 3 ;
colores = ColoresMatrix(ncolores);
for j=1:nloadstates*istep (1) +1
text(strain11(j),stress11(j),['',num2str(num(j))]);
end
sig=26;
stress11(sig)

```
ans =
    276.9497

```

function hplot = dibujar_criterio_dano1(ce,nu,q,tipo_linea,MDtype,n)
%* Inverse ce
ce_inv=inv(ce);
c11=ce_inv(1,1);
c22=ce_inv (2,2);
c12=ce_inv(1,2);
c21=c12;
c14=ce_inv(1,4);
c24=ce_inv (2,4);
if MDtype==1
tetha=[0:0.01:2*pi];
D=size(tetha);
m1=cos(tetha);
m2=sin(tetha);
Contador=D(1,2);
radio = zeros(1,Contador) ;
s1 = zeros(1,Contador) ;
s2 = zeros(1,Contador) ;
for i=1:Contador
radio(i)= q/sqrt([m1(i) m2(i) 0 nu*(m1(i) +m2(i))]*ce_inv*[m1(i) m2(i) 0 ...
nu*(m1(i)+m2(i))]');
s1(i)=radio(i)*m1(i);
s2(i)=radio(i)*m2(i);
end
hplot =plot(s1,s2,tipo_linea);
elseif MDtype==2
tetha=[0:0.01:pi/2];
D=size(tetha);
m1=cos(tetha);
m2=sin(tetha);
Contador=D(1,2);
radio = zeros(1,Contador+2) ;
s1 = zeros(1,Contador+2) ;
s2 = zeros(1,Contador+2) ;
for i=1:Contador
radio(i+1)= q/sqrt([m1(i) m2(i) 0 nu*(m1(i)+m2(i))]*ce_inv*[m1(i) m2(i) 0 ...
nu*(m1(i)+m2(i))]');
s1(i+1)=radio(i+1)*m1(i);
s2(i+1)=radio(i+1)*m2(i);
end
s1(1)= s1(2);
s2(1)=-200;
s1(Contador+2)=-100;
s2(Contador+2)=s1(2);

```
```

    hplot =plot(s1,s2,tipo_linea);
    elseif MDtype==3
tetha1=[0:0.01:pi/2];
tetha2=[pi:0.01:3*pi/2];
m1=[cos(tetha1) cos(tetha2)];
m2=[sin(tetha1) sin(tetha2)];
D=size(m1);
Contador=D (1,2);
radio = zeros(1,Contador+1) ;
s1 = zeros(1,Contador+1) ;
s2 = zeros(1,Contador+1) ;
for i=1:Contador/2
radio(i)= q/sqrt([m1(i) m2(i) 0 nu*(m1(i)+m2(i))]*ce_inv*[m1(i) m2(i) 0 ....
nu*(m1 (i) +m2 (i)) ]');
s1(i)=radio(i) *m1(i);
s2(i)=radio(i)*m2(i);
end
for i=Contador/2+1:Contador
radio(i)= q/sqrt([m1(i) m2(i) 0 nu*(m1(i)+m2(i))]*ce_inv*[m1(i) m2(i) 0 ...
nu*(m1(i) +m2(i)) ]');
s1(i)=radio(i) *m1(i)*n;
s2(i)=radio(i) *m2(i)*n;
end
%Close surface
s1(Contador+1)=s1(1);
hplot =plot(s1,s2,tipo_linea);
end
return

```
```

Not enough input arguments.
Error in dibujar_criterio_dano1 (line 4)
ce_inv=inv(ce);

```
```

function [sigma v,vartoplot,LABELPLOT,TIMEVECTOR]=damage main(Eprop,ntype,istep,strain,MDt
ype,n,TimeTotal)
global hplotSURF
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%
CONTINUUM DAMAGE MODEL
-----------------------
% Given the almansi strain evolution ("strain(totalstep,mstrain)") and a set of
% parameters and properties, it returns the evolution of the cauchy stress and other vari
ables
that are listed below.
INPUTS <<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<
----------------------------------------------------------------------
Eprop(1) = Young's modulus (E)
Eprop(2) = Poisson's coefficient (nu)
Eprop(3) = Hardening(+)/Softening(-) modulus (H)
Eprop(4) = Yield stress (sigma y)
Eprop(5) = Type of Hardening/Softening law (hard type)
0 --> LINEAR
1 --> Exponential
Eprop(6) = Rate behavior (viscpr)
0 --> Rate-independent (inviscid)
1 --> Rate-dependent (viscous)
Eprop(7) = Viscosity coefficient (eta) (dummy if inviscid)
Eprop(8) = ALPHA coefficient (for time integration), (ALPHA)
0<=ALPHA<=1 , ALPHA = 1.0 --> Implicit
ALPHA = 0.0 --> Explicit
(dummy if inviscid)
ntype = PROBLEM TYPE
1 : plane stress
2 : plane strain
3 : 3D
istep = steps for each load state (istep1,istep2,istep3)
strain(i,j) = j-th component of the linearized strain vector at the i-th
step, i = 1:totalstep+1
MDtype = Damage surface criterion %
1 : SYMMETRIC
2 : ONLY-TENSION
3 : NON-SYMMETRIC
n = Ratio compression/tension strength (dummy if MDtype is different from 3)
TimeTotal = Interval length
OUTPUTS <<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<<
1) sigma_v{itime}(icomp,jcomp) --> Component (icomp,jcomp) of the cauchy
stress tensor at step "itime"
REMARK: sigma v is a type of
variable called "cell array".

```
```

2) vartoplot{itime} --> Cell array containing variables one wishes to plot
vartoplot{itime}(1) = Hardening variable (q)
vartoplot{itime}(2) = Internal variable (r)%
3) LABELPLOT{ivar} --> Cell array with the label string for
variables of "varplot"
LABELPLOT{1} => 'hardening variable (q)'
LABELPLOT{2} => 'internal variable'
4) TIME VECTOR - >
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%%%%%%%%%
% SET LABEL OF "vartoplot" variables (it may be defined also outside this function)
%
LABELPLOT = {'hardening variable (q)','internal variable'};
E = Eprop(1) ; nu = Eprop (2) ;
viscpr = Eprop(6) ;
sigma_u = Eprop(4);
if ntype == 1
menu('PLANE STRESS has not been implemented yet','STOP');
error('OPTION NOT AVAILABLE')
elseif ntype == 3
menu('3-DIMENSIONAL PROBLEM has not been implemented yet','STOP');
error('OPTION NOT AVAILABLE')
else
mstrain = 4 ;
mhist = 6 ;
end
if viscpr == 1
% Comment/delete lines below once you have implemented this case
%
menu({'Viscous model has not been implemented yet. '; ...
'Modify files "damage main.m","rmap_dano1" ' ; ...
'to include this option'}, ...
'STOP');
error('OPTION NOT AVAILABLE')
else
end
totalstep = sum(istep) ;
% INITIALIZING GLOBAL CELL ARRAYS
% -------------------------------
sigma_v = cell(totalstep+1,1) ;
TIMEVECTOR = zeros(totalstep+1,1) ;
delta t = TimeTotal./istep/length(istep) ;
% Elastic constitutive tensor
```
```

% ------------------------------
[ce] = tensor_elastico1 (Eprop, ntype);
% Initz.
% -----
% Strain vector
% -------------
eps_n1 = zeros(mstrain,1);
% Historic variables
% hvar_n(1:4) --> empty
% hvar_n(5) = q --> Hardening variable
% hvar_n(6) = r --> Internal variable
hvar_n = zeros(mhist,1) ;
% INITIALIZING (i = 1) !!!!
% ***********i*
i = 1 ;
r0 = sigma u/sqrt(E);
hvar n(5) = r0; % r n
hvar_n(6) = r0; % q_n
eps_n1 = strain(i,:) ;
sigma_n1 =ce*eps_n1'; % Elastic
sigma v{i} = [sigma n1(1) sigma n1(3) 0;sigma n1(3) sigma n1(2) 0 ; 0 0 sigma n1(4)];
nplot = 3 ;
vartoplot = cell(1,totalstep+1) ;
vartoplot{i}(1) = hvar_n(6) ; % Hardening variable (q)
vartoplot{i}(2) = hvar_n(5) ; % Internal variable (r)
vartoplot{i}(3) = 1-hvar_n(6)/hvar_n(5) ; % Damage variable (d)
for iload = 1:length(istep)
% Load states
for iloc = 1:istep(iload)
i = i + 1 ;
TIMEVECTOR(i) = TIMEVECTOR(i-1)+ delta_t(iload) ;
% Total strain at step "i"
% ------------------------
eps_n1 = strain(i,:) ;
*****
%* DAMAGE MODEL
% %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
[sigma_n1,hvar_n,aux_var] = rmap_dano1(eps_n1,hvar_n,Eprop,ce,MDtype,n);
% PLOTTING DAMAGE SURFACE
if(aux_var(1)>0)
hplotSURF(i) = dibujar_criterio_dano1(ce, nu, hvar_n(6), 'r:',MDtype,n );
set(hplotSURF(i),'Color',[0 0 1],'LineWidth',1)
end
%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
%**********************************************************************
% GLOBAL VARIABLES
% ***************
% Stress
% ------
m_sigma=[sigma_n1(1) sigma_n1(3) 0;sigma_n1(3) sigma_n1(2) 0 ; 0 0 sigma_n1(4)];
sigma_v{i} = m_sigma ;
% VARIABLES TO PLOT (set label on cell array LABELPLOT)
% ----------------
vartoplot{i}(1) = hvar_n(6) ; % Hardening variable (q)
vartoplot{i}(2) = hvar_n(5) ; % Internal variable (r)

```
```

        vartoplot{i}(3) = 1-hvar n(6)/hvar n(5) ; % Damage variable (d)
    end
    end

```

Not enough input arguments.

Error in damage main (line 77)
\(\mathrm{E} \quad=\operatorname{Eprop}(1) ; \mathrm{nu}=\) Eprop (2) ;
```

function strain = calstrain_NI(istep,STRAIN)
% See select_path
mstrain = size(STRAIN,2) ;
strain = zeros(sum(istep)+1,mstrain) ;
acum = 0 ;
PNT = STRAIN(1,:) ;
for iloc = 1:length(istep)
INCSTRAIN = STRAIN(iloc+1,:)-STRAIN(iloc,:);
for i = 1:istep(iloc)
acum = acum + 1;
PNTb = PNT ;
% PNT = PNT+INCSTRAIN ;
PNT = PNT + INCSTRAIN/istep(iloc);
strain(acum+1,:) = PNT ;
end
end

```
```

Not enough input arguments.
Error in calstrain_NI (line 3)
mstrain = size(STRAIN,2) ;

```
```

