ASSINGMENT 1 COMPUTATIONAL SOLID MECHANICS

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PART1 (rate dependant models)

Rate independent+plain strain assumption

a)

1."NON symmetric tension-compression damage"

This implies changing *MDtype=3* in *main_no interactive*.

Next is changing the damage surface in *dibujar_criterio_dano1*. Now the surface is q=stress norm= $\tau_{\sigma} = \left[\theta + \frac{1-\theta}{n}\right] \sqrt{\sigma : \mathbb{C}^{-1} : \sigma}$, where n defined in main function (n=3) and $\left[\theta = \frac{1}{1-\sigma} + \frac{1}{2} \frac{\langle \sigma_i \rangle}{|\sigma_i|} = \frac{1}{1-\sigma} + \frac{1}{2} \frac{\langle \sigma_i \rangle}{|\sigma_i|}\right]$

tetha depending on main stresses.

This theta depends on McAuley and absolute value of main stresses, which can be divided in 4 ranges, for each of the quadrants.

For plotting we use the " σ_1 =r θ cos θ & σ_1 =r(θ)cos(θ) polar coordinates. (radius depending on θ is the key) and vector "s1" and "s2" sum include point son first and third quadrant. Lines on second and fourth quadrant are just made joining to points attached.



For calculating the stresses must be done on *modelos_de_dano1*, *Tangent constitutive operator* $\langle \langle , \rangle$, which is considered constant and given by ν and **E**.

Quadrant 1 σ_1 >0; σ_2 >0; θ_1 =1 Quadrant 2 σ_1 >0; σ_2 <0; θ_2 = $\sigma_1/(\sigma_1+\sigma_2)$ Quadrant 3 σ_1 <0; σ_2 <0; θ_3 =0 Quadrant 4 σ_1 <0; σ_2 >0; θ_4 = $\sigma_2/(\sigma_1+\sigma_2)$

we define non-symmetric factor as $F=(\theta + (1-\theta)/n)$.

Quadrant 1 θ_1 =1; F=1 Quadrant 2 $\theta_2 = \sigma_1/(\sigma_1 + \sigma_2) = \cos\theta/(\cos\theta + \sin\theta)$; F=(θ_2 + (1- θ_2 /n) Quadrant 3 θ_3 =0; Quadrant 4 $\theta_4 = \sigma_2/(\sigma_1 + \sigma_2) = \sin\theta/(\cos\theta + \sin\theta)$; F=(θ_2 + (1- θ_4)/n)

Strain norm will be same as symmetric case, divided by this factor, which depends on main stresses.

2."Tensile-only" damage model

Plotting is quite trivial, just taking profit of first quadrant and plotting two straight lines. This must be done at *dibujar_criterio_dano1*.



Again, for calculating the stresses must be done on *modelos_de_dano1*, *Tangent constitutive operator* \mathcal{C} , which is considered constant and given by v and **E**.

3d quadrant

We assume Strain norm =0 for other quadrants than the first one.

b)

Implement linear and exponential hardening/softening (H<0,H>0) Linear

Linear is already implemented. To implement exponential will be necessary to modify *rmap_dano1*, which calculates the stress path depending on hardening function assumption.

Only loading variant will take into account the hardening function.

It's remarkable that of H<0, the elastic domain diminishes, and if it's H>0 it increases (e.g. metal cases). In this last case the damage leds to a more resistance a posterior stress.

Exponential

when: $q_{inf} < r_0$ -->elastic domain diminishes $q_{inf} > r_0$, it increases. $q_{inf} = r_0$ Elastic domain remains the same

it's been detected that when it $q_{inf} > r_0$, "A" *takes an important role* in correct behaviour of simulation.

Hypothesis: It has to be taken into account that $aux_var(6)=q_{n+1}/r_{n+1}$ has to be bigger than q_n/r_n in order to damage never decrease.

With q_{inf}=2 and A=2:

Examples on 4 combinations:



Exponential symmetric case





Non sym exponential







Both cases, **more damage in linear,** though elastic domain does increases in exponential vs linear.

For each case obtain stress space and stress strain

Considering *EXPONENTIAL HARDENING/SOFTENING* in order to linear/non linear behaviour to be more obvious.

1. $\Delta \sigma_1^{(1)} = \alpha ; \Delta \sigma_2^{(1)} = 0$ $\Delta \sigma_1^{(2)} = -\beta ; \Delta \sigma_2^{(2)} = 0$ $\Delta \sigma_1^{(3)} = \gamma ; \Delta \sigma_3^{(3)} = 0$

SIGMAP=($\alpha 0, \alpha - \beta 0, \alpha - \beta + \gamma 0$)



<u>First path 1-11</u>

1 to 5 Elastic domain. No damage. Linear behaviour. REACHES damage surface. 5 to 11 Load. Damage. Damage Surface increases.

First path 11-21

11 to 21 Unload. No damage. Elastic behaviour (E_d)

First path 21-31

21-27 Elastic domain. No damage. Linear behaviour. REACHES damage surface. 27 to 31 Load. Damage Surface (already increased) increases more. reaches at σ_2 =284 vs σ_2 =200 of point 5.

• Non Symmetric tension-compression: Same

C)

- tension-only case:Same
- 2. $\Delta \sigma_1^{(1)} = \alpha ; \Delta \sigma_2^{(1)} = 0$ $\Delta \sigma_1^{(2)} = -\beta ; \Delta \sigma_2^{(2)} = -\beta$ $\Delta \sigma_1^{(3)} = \gamma ; \Delta \sigma_3^{(3)} = \gamma$

SIGMAP=($\alpha 0, \alpha - \beta - \beta, \alpha - \beta + \gamma - \beta + \gamma$)



First path 1-11

1 to 8 Elastic domain. No damage. Linear behaviour. REACHES damage surface. 8 to 11 Load. Damage. Damage Surface increases.

First path 11-21

11 to 21 Unload. No damage. Elastic behaviour (E_d)

First path 21-31

21-25 Elastic domain. No damage. Linear behaviour. REACHES damage surface.25 to 31 Load. Damage Surface (already increased) increases more.



Non Symmetric tension-compression

Very similar to symmetric case:

<u>First path 1-11</u>

1 to 8 Elastic domain. No damage. Linear behaviour. REACHES damage surface. 8 to 11 Load. Damage. Damage Surface increases.

<u>First path 11-21</u> 11to 21 Unload. No damage. Elastic behaviour (E_d)

First path 21-31

21-26 Elastic domain. No damage. Linear behaviour. REACHES damage surface. 26 to 31 Load. Damage Surface (already increased) increases more. **Reaches surface at** σ_2 =287 vs σ_2 =158 of point 26.





First path 1-11 1 to 8 *Elastic domain. No damage. Linear behaviour. REACHES damage surface.* 8 to 11 Load. Damage. Damage Surface increases.

<u>First path 11-21</u> 11 to 21 Unload. No damage. Elastic behaviour (E_d)

First path 21-31

21-26 Elastic domain. No damage. Linear behaviour. REACHES damage surface. 26 to 31 Load. Damage Surface (already increased) increases more. Reaches surface at σ_2 =288 vs σ_2 =210 of point 19-20. 3. $\Delta \sigma_1^{(1)} = \alpha ; \Delta \sigma_2^{(1)} = \alpha$ $\Delta \sigma_1^{(2)} = -\beta ; \Delta \sigma_2^{(2)} = -\beta$ $\Delta \sigma_1^{(3)} = \gamma ; \Delta \sigma_3^{(3)} = \gamma$

SIGMAP=($\alpha \alpha, \alpha - \beta \alpha - \beta, \alpha - \beta + \gamma \alpha - \beta + \gamma$)



First path 1-11 1 to 7 *Elastic domain. No damage. Linear behaviour. REACHES damage surface.* 7 to 11 Load. Damage. Damage Surface increases.

First path 11-21

11 to 21 Unload. No damage. Elastic behaviour (E_d)

First path 21-31

21-22 Elastic domain. No damage. Linear behaviour. REACHES damage surface.22 to 31 Load. Damage Surface (already increased) increases more.

- Non Symmetric tension-compression: Same
- tension-only case:Same

ANEXO 1

```
function [rtrial] = Modelos de dano1 (MDtype,ce,eps n1,n)
  if (MDtype==1)
                       %* Symmetric
   rtrial= sqrt(eps_n1*ce*eps_n1');
   elseif (MDtype==2) %* Only tension
  sigma=ce*eps n1';
  sigmal=sigma(1);
  sigma2=sigma(2);
  if (sigma1>0) && (sigma2>0)
  rtrial= sqrt(eps n1*ce*eps n1')
  elseif (sigma1<0) && (sigma2<0)</pre>
  rtrial=0;
  elseif ((sigma1<0) && (sigma2>0)) %!!!!
   rtrial=0;
  elseif ((sigma1>0)&&(sigma2<0)) %!!!!</pre>
    rtrial=0;
  end
   elseif (MDtype==3) %*Non-symmetric
  sigma=ce*eps n1';
  sigma1=sigma(1);
  sigma2=sigma(2);
  if (sigma1>0) && (sigma2>0)
  rtrial= sqrt(eps_n1*ce*eps_n1')
  elseif (sigma1<0) && (sigma2<0)</pre>
  rtrial= sqrt(eps n1*ce*eps n1')*n;
  elseif ((sigma1<0) && (sigma2>0))
       tetha=sigma2/(sigma1+sigma2);
       F=tetha+(1-tetha)/n;
       rtrial= sqrt(eps n1*ce*eps n1')/F;
  elseif ((sigma1>0)&&(sigma2<0))%%%%%%%%aqui!!!!!</pre>
       tetha=sigma1/(sigma1+sigma2);
       F=tetha+(1-tetha)/n;
       rtrial= sqrt(eps n1*ce*eps n1')/F;
  end
  end
return
```

```
function plotcurvesNEW(DATA,vpx,vpy,LABELPLOT,vartoplot)
% Plot stress vs strain (callback function)
§ _____
% PLOTTING
ncolores = 3;
colores = ColoresMatrix(ncolores);
markers = MarkerMatrix(ncolores) ;
subplot(2,2,3)
title('DAMAGE')
hold on
grid on
xlabel(vpx);
ylabel(vpy);
switch vpx
   case 'STRAIN 1'
       strx = 'X(i) = DATA.strain(i,1);' ;
       %strx = 'X(i) = max(DATA.strain(i,1),DATA.strain(i,2));' ;
   case 'STRAIN 2'
       strx = 'X(i) = DATA.strain(i,2);' ;
       %strx = 'X(i) = min(DATA.strain(i,1),DATA.strain(i,2));' ;
   case '|STRAIN 1|'
       strx = 'X(i) = abs(DATA.strain(i,1));';
       %strx = 'X(i) = abs(max(DATA.strain(i,1),DATA.strain(i,2)));' ;
   case '|STRAIN 2|'
       strx = 'X(i) = abs(DATA.strain(i,2));' ;
       %strx = 'X(i) = abs(min(DATA.strain(i,1),DATA.strain(i,2)));';
   case 'norm(STRAIN)'
       strx = 'X(i) =sqrt((DATA.strain(i,1))^2 + (DATA.strain(i,2))^2)) ;';
   case 'TIME'
       strx = 'X(i) =DATA.TIMEVECTOR(i) ;';
   otherwise
       for iplot = 1:length(LABELPLOT)
           switch vpx
              case LABELPLOT{iplot}
                  strx = ['X(i) = vartoplot{i}(',num2str(iplot),');'];
           end
       end
end
X = 0;
for i = 1:size(DATA.strain,1)
   eval(strx) ;
end
% DATA Y
8 _____
switch vpy
```

```
case 'STRESS 1'
        stry = 'Y(i) = DATA.sigma v{i}(1,1);';
        %stry = 'Y(i) = max(DATA.sigma v{i}(1,1),DATA.sigma v{i}(2,2));';
    case 'STRESS 2'
       stry = 'Y(i) = DATA.sigma v\{i\}(2,2);';
        %stry = 'Y(i) = min(DATA.sigma v{i}(1,1), DATA.sigma v{i}(2,2));';
    case '|STRESS 1|'
       %stry = 'Y(i) = abs(max(DATA.sigma_v{i}(1,1),DATA.sigma_v{i}(2,2)));';
       stry = 'Y(i) = abs(DATA.sigma v{i}(1,1));';
    case '|STRESS 2|'
        %stry = 'Y(i) = abs(min(DATA.sigma v{i}(1,1),DATA.sigma v{i}(2,2)));';
       stry = 'Y(i) = abs(DATA.sigma v{i}(2,2));';
    case 'norm(STRESS)'
       stry = 'Y(i) = sqrt((DATA.sigma_v{i}(1,1))^2+(DATA.sigma_v{i}(2,2))^2);';
    case 'DAMAGE VAR.'
        stry = 'Y(i) = sqrt((DATA.sigma v{i}(1,1))^2+(DATA.sigma v{i}(2,2))^2);';
    otherwise
        for iplot = 1:length(LABELPLOT)
            switch vpy
                case LABELPLOT{iplot}
                    stry = ['Y(i) = vartoplot{i}(',num2str(iplot),');'];
            end
        end
end
Y = 0;
for i = 1:length(DATA.sigma v)
   try
        eval(stry);
    end
end
plot(X,Y,'Marker',markers{1},'Color',colores(1,:));
for i=1:length(X)
    text(X(i),Y(i),num2str(i));
end
```

```
Error in plotcurvesNEW (line 20)
xlabel(vpx);
```

```
function strain =PlotIniSurf(YOUNG M, POISSON, YIELD STRESS, SIGMAP, ntype, MDtype, n, istep)
Eprop=[YOUNG M POISSON 0 YIELD STRESS];
sigma u =YIELD STRESS ;
E = YOUNG M ;
nu = POISSON ;
2*
     Evaluar el tensor constitutivo el�stico (Matriz de Hooke)
                                                                       8*
     Llamado de Rutina tensor elasticol
                                                                      응*
응*
[ce] = tensor elastico1 (Eprop, ntype);
                                 *****
2*****************
%*
                                                                       ે *
     Dibujo de la superficie de da�o
8*
     Llamado de Rutina dibujar criterio citerio da�ol
                                                                       응*
figure(1);
set(1, 'Name', 'ANALYSIS OF A DAMAGE MODEL (GAUSS POINT LEVEL)')
hold on;
%dbstop('122')
subplot(1,2,1);
title('Damage surface (principal stresses axes)')
xlabel('\sigma {1}')
ylabel('\sigma_{2}')
hold on;
grid on;
pbaspect([2 1 1]); %%escala ejes es igual
q=sigma u/sqrt(E);
hplot = dibujar criterio dano1(ce, nu, q , 'b-', MDtype,n );
$$$$$$
if ntype == 2
   SIGMAP = [0 0; SIGMAP] ;
   mstrain = 4;
   hplotquiver = [] ;
   STRAIN = zeros(size(SIGMAP,1),4);
   for iloc = 1:size(SIGMAP, 1) -1
      SSS =SIGMAP(iloc,:);
      sigma bef=[SSS(1) SSS(2) 0 nu*(SSS(1)+SSS(2))];
      SSS =SIGMAP(iloc+1,:);
      sigma_0=[SSS(1) SSS(2) 0 nu*(SSS(1)+SSS(2))];
      8
           hplotquiver(end+1) = plot([sigma bef(1) sigma 0(1)],[sigma bef(2) sigma 0(2)
]) ;
      plot( sigma 0(1), sigma 0(2), 'b*')
      text( sigma 0(1), sigma 0(2),['P=',num2str(iloc)]);
      strain di =(inv(ce)*sigma 0')';
      STRAIN(iloc+1,:) = strain di ;
```

```
end
end
% PLOTTING (PATH)
% ********
% Divide SIGMAP{end} - SIGMAP{end-1} in istep1 steps
hplotp = [];
[ hplotp hplot1]=plotpathNI(SIGMAP,istep);
[strain] = calstrain_NI(istep,STRAIN) ;
```

```
Not enough input arguments.
```

```
Error in PlotIniSurf (line 6)
Eprop=[YOUNG M POISSON 0 YIELD STRESS];
```

```
function [hplotp, hplotl]=plotpathNI(SIGMAP,istep)
% See select path
% It plots stress path
% Plot iloc-th stretch
% -----
PNT = SIGMAP(1,:);
hplotp = plot(PNT(1), PNT(2), 'ro');
hplotl = [];
for iloc = 1:size(SIGMAP,1)-1
   INCSIGMA = SIGMAP(iloc+1,:)-SIGMAP(iloc,:) ;
   for i = 1:istep(iloc)
       PNTb = PNT ;
       % PNT = PNT+INCSIGMA* ;
       PNT = PNT+INCSIGMA/(istep(iloc));
       LINE = [PNTb ; PNT] ;
       hplotp(end+1) = plot(PNT(1), PNT(2), 'ro');
       hplotl(end+1) = plot(LINE(:,1) ,LINE(:,2),'r','LineWidth',1,'LineStyle','--');
   end
end
```

```
Error in plotpathNI (line 7)
PNT = SIGMAP(1,:) ;
```

```
function [sigma n1, hvar n1, aux var] = rmap dano1 (eps n1, hvar n, Eprop, ce, MDtype, n)
+
2*
8*
       Integration Algorithm for a isotropic damage model
응*
응*
응*
       [sigma n1, hvar n1, aux var] = rmap dano1 (eps n1, hvar n, Eprop, ce)
응*
             eps_n1(4) strain (almansi) step n+1
%* INPUTS
                    vector R4 (exx eyy exy ezz)
응*
             hvar n(6) internal variables , step n
8*
응*
                    hvar n(1:4) (empty)
8*
                    hvar n(5) = r; hvar n(6) = q
8*
             Eprop(:) Material parameters
8*
             ce(4,4) Constitutive elastic tensor
2*
응*
                                                    *
             sigma n1(4) Cauchy stress , step n+1
%* OUTPUTS:
             hvar_n(6) Internal variables , step n+1
8*
*
응*
             aux var(3) Auxiliar variables for computing const. tangent tensor
*
hvar n1 = hvar n;
r n = hvar n(5);
q_n
   = hvar n(6);
    = Eprop(1);
Ε
nu = Eprop(2);
H = Eprop(3);
sigma u = Eprop(4);
hard type = Eprop(5);
%* initializing
                                         ુ *
r0 = sigma u/sqrt(E);
zero q=1.d-6*r0;
% if(r_n<=0.d0)
% r n=r0;
% q_n=r0;
% end
%* Damage surface
                                                   8*
[rtrial] = Modelos de_dano1 (MDtype,ce,eps_n1,n);
*****
Ver el Estado de Carga
                                                    8*
8*
  ----> fload=0 : elastic unload
                                                    8*
2*
%* -----> fload=1 : damage (compute algorithmic constitutive tensor)
                                                   8*
fload=0;
```

```
if(rtrial > r_n)
 %* Loading
  fload=1;
  delta_r=rtrial-r_n;
  r n1= rtrial ;
  if hard_type == 0
     % Linear
     q n1= q n+ H*delta r; %remember that H=0,1, wich is >0, thus hardening
  else
     %exponential!!!!!!
     A=6; %if A=0; Elastic domain remains the same
     qinf=2; %qinf<0-->elastic domain diminishes, qinf>r0, it increases.
     q n1=qinf-(qinf-q n) *exp(A*(1-rtrial/r n));
  end
  if(q_n1<zero_q)</pre>
     q n1=zero q;
  end
else
  %* Elastic load/unload
  fload=0;
  r_n1= r_n ;
  q_n1= q_n ;
end
% Damage variable
% _____
dano_n1 = 1.d0-(q_n1/r_n1);
% Computing stress
8 ****
sigma n1 =(1.d0-dano n1)*ce*eps n1';
%hold on
%plot(sigma n1(1), sigma n1(2), 'bx')
*****
                                                   ે *
%* Updating historic variables
% hvar n1(1:4) = eps n1p;
hvar_n1(5) = r_n1 ;
hvar n1(6) = q n1;
%* Auxiliar variables
                                                          8*
aux var(1) = fload;
aux var(2) = q n1/r n1;
%*aux var(3) = (q_n1-H*r_n1)/r_n1^3;
8******
                                 *****
```

```
function [ce] = tensor elastico1 (Eprop, ntype)
                          *****
8***
 Elastic constitutive tensor
2*
                                               2*
%
           G ----> Shear modulus
응*
                                               ક*
           K ----> Bulk modulus
응*
                                               ક*
G=Eprop(1)/(2*(1+Eprop(2)));
K = Eprop(1) / (3*(1-2*Eprop(2)));
                *******
8*********
         * * * * * * * * * * * *
if(ntype==1)
                    % Plane stress
elseif(ntype==2)
                      % Plane strain
    ce = zeros(4, 4);
                      % Init.
    C1=K+(4.0D0/3.0D0)*G;
    C2=K-(2.0D0/3.0D0)*G;
    ce(1,1) = C1;
    ce(2,2)=C1;
    ce(4,4)=C1;
    ce(1,2)=C2;
    ce(1, 4) = C2;
    ce(2, 4) = C2;
    ce(2,1)=C2;
    ce(4,1)=C2;
    ce(4,2)=C2;
    ce(3,3) = G;
elseif(ntype==4)
                      % Tres Dimensiones
end
return
```

```
Not enough input arguments.
```

```
Error in tensor_elastico1 (line 11)
G=Eprop(1)/(2*(1+Eprop(2)));
```

Contents

Plot Initial Damage Surface and effective stress path

```
clc
clear all
% Program for modelling damage model
% (Elemental gauss point level)
응 _____
% Developed by J.A. Hdez Ortega
% 20-May-2007, Universidad Politécnica de Cataluña
%profile on
≗ ************
% INPUTS
8 ******
% YOUNG's MODULUS
8 _____
YOUNG M = 20000;
% Poisson's coefficient
8 _____
POISSON = 0.3;
% Hardening/softening modulus
§_____
HARDSOFT MOD = 0.1;
% Yield stress
8 _____
YIELD STRESS = 200;
% Problem type TP = {'PLANE STRESS', 'PLANE STRAIN', '3D'}
8 ----- = 1
                           =2
                                    =3
8 _____
ntype= 2 ;
% Model PTC = {'SYMMETRIC', 'TENSION', 'NON-SYMMETRIC'};
           = 1 = 2 = 3
00
8 -----
MDtype =1;
% Ratio compression strength / tension strength
8 _____
n = 3;
% SOFTENING/HARDENING TYPE
° -----
HARDTYPE = 'EXP' ; %{LINEAR, EXPONENTIAL} %diferente de linear es suficiente
% VISCOUS/INVISCID
8 -----
VISCOUS = 'NO' ;
% Viscous coefficient ----
oc _____
eta = 0.3;
% TimeTotal (initial = 0) ----
8 -----
TimeTotal = 10 ; ;
% Integration coefficient ALPHA
% _____
ALPHA COEFF = 0.5;
% Points -----
```

```
8 _____
nloadstates = 3 ;
SIGMAP = zeros(nloadstates,2) ;
8{
SIGMAP(1,:) = [300 400];
SIGMAP(2,:) = [500 \ 400];
SIGMAP(3,:) = [500 0];
8}
Su=YIELD STRESS;
alfa=[300 150 600];
$$$$$$$$$$$$$$$$$$$$$$
%tipo de caso del problema c
                 num='3';
switch num
   case 'def'
   SIGMAP(1,:) = [300 \ 400];
   SIGMAP(2,:) = [500 \ 400];
   SIGMAP(3,:) = [500 0];
   case '1'
   SIGMAP(1,:) =[alfa(1) 0];
   SIGMAP(2,:) =[alfa(1)-alfa(2) 0];
   SIGMAP(3,:) =[alfa(1)-alfa(2)+alfa(3) 0];
   case '2'
   SIGMAP(1,:) = [alfa(1) 0];
   SIGMAP(2,:) =[alfa(1)-alfa(2) (-alfa(2))];
   SIGMAP(3,:) =[alfa(1)-alfa(2)+alfa(3) (-alfa(2)+alfa(3))];
   otherwise
   SIGMAP(1,:) =[alfa(1) alfa(1)];
   SIGMAP(2,:) =[alfa(1)-alfa(2) alfa(1)-alfa(2)];
   SIGMAP(3,:) = [alfa(1) - alfa(2) + alfa(3) alfa(1) - alfa(2) + alfa(3)];
end
% Number of time increments for each load state
§ _____
istep = 10*ones(1,nloadstates) ;
% VARIABLES TO PLOT
vpx = 'TIME' ; % AVAILABLE OPTIONS: 'STRAIN 1', 'STRAIN 2'
                '|STRAIN 1|', '|STRAIN 2|'
8
% 'norm(STRAIN)', 'TIME'
vpy = 'damage variable (d) ' % AVAILABLE OPTIONS: 'STRESS 1', 'STRESS 2'
                 '|STRESS 1|', '|STRESS 2|'
00
% 'norm(STRESS)', 'TIME', 'DAMAGE VAR.', 'hardening variable (q)', 'damage variable (d)'
% 'internal variable (r)'
% 3) LABELPLOT{ivar}
                            --> Cell array with the label string for
                              variables of "varplot"
0
2
LABELPLOT = { 'hardening variable (q) ', 'internal variable (r) ', 'damage variable (d) '};
```

Plot Initial Damage Surface and effective stress path

```
strain history = PlotIniSurf(YOUNG M, POISSON, YIELD STRESS, SIGMAP, ntype, MDtype, n, istep);
E = YOUNG_M
nu = POISSON
                  ;
                       ;
sigma u = YIELD STRESS ;
switch HARDTYPE
   case 'LINEAR'
       hard type = 0 ;
   otherwise
      hard_type = 1 ;
end
switch VISCOUS
   case 'YES'
       viscpr = 1
                     ;
   otherwise
      viscpr = 0 ;
end
Eprop = [E nu HARDSOFT MOD sigma u hard type viscpr eta ALPHA COEFF]
                                                                                   ;
% DAMAGE MODEL
% _____
[sigma v,vartoplot,LABELPLOT out,TIMEVECTOR]=damage main(Eprop,ntype,istep,strain history,
MDtype,n,TimeTotal);
try; LABELPLOT;catch;LABELPLOT = LABELPLOT_out ; end ;
% PLOTTING
§ _____
ncolores = 3;
colores = ColoresMatrix(ncolores);
markers = MarkerMatrix(ncolores) ;
hplotLLL = [] ;
for i = 2:length(sigma v)
    stress_eig = sigma_v{i} ; %eigs(sigma_v{i}) ;
    tstress_eig = sigma_v{i-1}; %eigs(sigma_v{i-1}) ;
    hplotLLL(end+1) = plot([tstress_eig(1,1) stress_eig(1,1) ],[tstress_eig(2,2) stress ei
g(2,2)],'LineWidth',2,'color',colores(1,:),'Marker',markers{1},'MarkerSize',2);
```

```
plot(stress eig(1,1),stress eig(2,2),'bx')
    text(stress_eig(1,1),stress_eig(2,2),num2str(i))
   % SURFACES
   § ____
end
% % SURFACES
8 8 -----
% if(aux var(1)>0)
    hplotSURF(i) = dibujar criterio danol(ce, nu, hvar n(6), 'r:',MDtype,n);
8
     set(hplotSURF(i), 'Color', [0 0 1], 'LineWidth', 1);
00
% end
DATA.sigma_v = sigma_v
                           ;
DATA.vartoplot = vartoplot
                             ;
DATA.LABELPLOT = LABELPLOT ;
DATA.TIMEVECTOR = TIMEVECTOR ;
DATA.strain = strain_history ;
%plotcurvesNEW(DATA,vpx,vpy,LABELPLOT,vartoplot) ;
subplot(1,2,2)
$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$$
set(1, 'Name', 'ANALYSIS OF A DAMAGE MODEL (GAUSS POINT LEVEL)')
hold on;
title('STRESS-STRAIN')
xlabel('STRAIN')
ylabel('STRESS')
hold on;
grid on;
strain11=strain_history(:,1);
stress11=zeros(nloadstates*istep(1)+1,1);
num=zeros(1,nloadstates*istep(1)+1);
for i=1:31
stress11(i) = sigma_v{i}(1,1);
num(i)=i;
end
size(strain11);
size(stress11);
plot(strain11, stress11, 'r');
```

```
ncolores = 3 ;
colores = ColoresMatrix(ncolores);
for j=1:nloadstates*istep(1)+1
text(strain11(j),stress11(j),['',num2str(num(j))]);
end
sig=26;
stress11(sig)
```

ans =

276.9497



```
function hplot = dibujar criterio danol(ce,nu,q,tipo linea,MDtype,n)
응*
                                                                                     8*
         Inverse ce
ce_inv=inv(ce);
c11=ce inv(1,1);
c22=ce_inv(2,2);
c12=ce inv(1,2);
c21=c12;
c14=ce inv(1,4);
c24=ce_inv(2,4);
if MDtype==1
   tetha=[0:0.01:2*pi];
   D=size(tetha);
   m1=cos(tetha);
   m2=sin(tetha);
   Contador=D(1,2);
   radio = zeros(1,Contador) ;
   s1 = zeros(1,Contador);
   s2 = zeros(1,Contador) ;
    for i=1:Contador
       radio(i) = q/sqrt([m1(i) m2(i) 0 nu*(m1(i)+m2(i))]*ce inv*[m1(i) m2(i) 0 ...
            nu*(m1(i)+m2(i))]');
       s1(i)=radio(i)*m1(i);
       s2(i)=radio(i)*m2(i);
    end
    hplot =plot(s1,s2,tipo linea);
elseif MDtype==2
 tetha=[0:0.01:pi/2];
    D=size(tetha);
   m1=cos(tetha);
   m2=sin(tetha);
   Contador=D(1,2);
   radio = zeros(1,Contador+2) ;
   s1 = zeros(1,Contador+2) ;
    s2 = zeros(1, Contador+2);
    for i=1:Contador
       radio(i+1) = q/sqrt([m1(i) m2(i) 0 nu*(m1(i)+m2(i))]*ce_inv*[m1(i) m2(i) 0 ...
            nu*(m1(i)+m2(i))]');
       s1(i+1) = radio(i+1) * m1(i);
       s2(i+1)=radio(i+1)*m2(i);
    end
    s1(1) = s1(2);
    s2(1) = -200;
    s1(Contador+2) = -100;
    s2(Contador+2) = s1(2);
```

```
hplot =plot(s1,s2,tipo_linea);
elseif MDtype==3
   tetha1=[0:0.01:pi/2];
   tetha2=[pi:0.01:3*pi/2];
   m1=[cos(tetha1) cos(tetha2)];
   m2=[sin(tetha1) sin(tetha2)];
    D=size(m1);
   Contador=D(1,2);
   radio = zeros(1,Contador+1) ;
   s1 = zeros(1,Contador+1);
    s2 = zeros(1,Contador+1);
    for i=1:Contador/2
        radio(i) = q/sqrt([m1(i) m2(i) 0 nu*(m1(i)+m2(i))]*ce_inv*[m1(i) m2(i) 0 ...
            nu*(m1(i)+m2(i))]');
       s1(i) = radio(i) *m1(i);
       s2(i)=radio(i) *m2(i);
    end
    for i=Contador/2+1:Contador
       radio(i) = q/sqrt([m1(i) m2(i) 0 nu*(m1(i)+m2(i))]*ce_inv*[m1(i) m2(i) 0 ...
            nu*(m1(i)+m2(i))]');
       s1(i) = radio(i) *m1(i) *n;
        s2(i)=radio(i)*m2(i)*n;
    \operatorname{end}
    %Close surface
    s1(Contador+1) = s1(1);
    hplot =plot(s1,s2,tipo_linea);
end
return
```

```
Error in dibujar_criterio_dano1 (line 4)
ce inv=inv(ce);
```

```
function [sigma v,vartoplot,LABELPLOT,TIMEVECTOR]=damage main(Eprop,ntype,istep,strain,MDt
ype,n,TimeTotal)
global hplotSURF
8888888888
% CONTINUUM DAMAGE MODEL
° _____
% Given the almansi strain evolution ("strain(totalstep,mstrain)") and a set of
% parameters and properties, it returns the evolution of the cauchy stress and other vari
ables
% that are listed below.
2
of
% Eprop(1) = Young's modulus (E)
% Eprop(2) = Poisson's coefficient (nu)
% Eprop(3) = Hardening(+)/Softening(-) modulus (H)
% Eprop(4) = Yield stress (sigma y)
% Eprop(5) = Type of Hardening/Softening law (hard type)
          0 --> LINEAR
%
         1 --> Exponential
8
% Eprop(6) = Rate behavior (viscpr)
00
          0 --> Rate-independent (inviscid)
          1 --> Rate-dependent (viscous)
엉
00
% Eprop(7) = Viscosity coefficient (eta) (dummy if inviscid)
% Eprop(8) = ALPHA coefficient (for time integration), (ALPHA)
          0<=ALPHA<=1 , ALPHA = 1.0 --> Implicit
00
                      ALPHA = 0.0 --> Explicit
8
0
          (dummy if inviscid)
8
% ntype = PROBLEM TYPE
         1 : plane stress
2
8
          2 : plane strain
          3 : 3D
2
6
% istep = steps for each load state (istep1,istep2,istep3)
% strain(i,j) = j-th component of the linearized strain vector at the i-th
00
            step, i = 1:totalstep+1
8
% MDtype
          = Damage surface criterion %
         1 : SYMMETRIC
8
          2 : ONLY-TENSION
0
9
          3 : NON-SYMMETRIC
2
0
          = Ratio compression/tension strength (dummy if MDtype is different from 3)
% n
00
% TimeTotal = Interval length
0
%
 OUTPUTS <<<<<<<<<<<<<<<<<>>
8
     _____
% 1) sigma_v{itime}(icomp,jcomp) --> Component (icomp,jcomp) of the cauchy
8
                             stress tensor at step "itime"
00
                             REMARK: sigma v is a type of
00
                              variable called "cell array".
90
00
```

```
% 2) vartoplot{itime}
                             --> Cell array containing variables one wishes to plot
00
                               _____
   vartoplot{itime}(1) = Hardening variable (q)
90
00
  vartoplot{itime}(2) = Internal variable (r)%
2
  3) LABELPLOT{ivar}
                             --> Cell array with the label string for
00
                              variables of "varplot"
8
0
        LABELPLOT{1} => 'hardening variable (g)'
8
         LABELPLOT{2} => 'internal variable'
8
8
2
\% 4) TIME VECTOR - >
% SET LABEL OF "vartoplot" variables (it may be defined also outside this function)
§ _____
LABELPLOT = { 'hardening variable (q) ', 'internal variable' };
   = Eprop(1) ; nu = Eprop(2) ;
Ε
viscpr = Eprop(6);
sigma_u = Eprop(4);
if ntype == 1
   menu('PLANE STRESS has not been implemented yet','STOP');
   error ('OPTION NOT AVAILABLE')
elseif ntype == 3
   menu('3-DIMENSIONAL PROBLEM has not been implemented yet','STOP');
   error('OPTION NOT AVAILABLE')
else
   mstrain = 4 ;
   mhist = 6
                ;
end
if viscpr == 1
   % Comment/delete lines below once you have implemented this case
   menu({'Viscous model has not been implemented yet. '; ...
       'Modify files "damage main.m", "rmap dano1" ' ; ...
       'to include this option'}, ...
       'STOP');
   error('OPTION NOT AVAILABLE')
else
end
totalstep = sum(istep) ;
% INITIALIZING GLOBAL CELL ARRAYS
§ _____
sigma v = cell(totalstep+1,1) ;
TIMEVECTOR = zeros(totalstep+1,1) ;
delta t = TimeTotal./istep/length(istep) ;
```

```
§ _____
[ce] = tensor_elastico1 (Eprop, ntype);
% Initz.
8 _____
% Strain vector
§ _____
eps_n1 = zeros(mstrain,1);
% Historic variables
\% hvar n(1:4) --> empty
\% hvar n(5) = q --> Hardening variable
  hvar_n(6) = r --> Internal variable
hvar n = zeros(mhist,1) ;
% INITIALIZING (i = 1) !!!!
8 *********i*
i = 1;
r0 = sigma u/sqrt(E);
hvar n(5) = r0; % r n
hvar n(6) = r0; % q n
eps_n1 = strain(i,:) ;
sigma n1 =ce*eps n1'; % Elastic
sigma v{i} = [sigma n1(1) sigma n1(3) 0;sigma n1(3) sigma n1(2) 0; 0 0 sigma n1(4)];
nplot = 3;
vartoplot = cell(1,totalstep+1) ;
vartoplot{i}(1) = hvar_n(6) ; % Hardening variable (q)
vartoplot{i}(2) = hvar n(5) ; % Internal variable (r)
vartoplot{i}(3) = 1-hvar_n(6)/hvar_n(5); % Damage variable (d)
for iload = 1:length(istep)
   % Load states
   for iloc = 1:istep(iload)
      i = i + 1;
      TIMEVECTOR(i) = TIMEVECTOR(i-1) + delta t(iload) ;
      % Total strain at step "i"
      <u> ୧</u>
      eps n1 = strain(i,:) ;
                                2************
*****
      %* DAMAGE MODEL
      [sigma_n1,hvar_n,aux_var] = rmap_dano1(eps_n1,hvar_n,Eprop,ce,MDtype,n);
      % PLOTTING DAMAGE SURFACE
      if(aux var(1) > 0)
         hplotSURF(i) = dibujar criterio dano1(ce, nu, hvar n(6), 'r:',MDtype,n );
          set(hplotSURF(i), 'Color', [0 0 1], 'LineWidth', 1)
                                                                     ;
      end
      % GLOBAL VARIABLES
      & ***********
      % Stress
      m_sigma=[sigma_n1(1) sigma_n1(3) 0;sigma_n1(3) sigma_n1(2) 0 ; 0 0 sigma_n1(4)];
      sigma v{i} = m sigma ;
      % VARIABLES TO PLOT (set label on cell array LABELPLOT)
      § _____
      vartoplot{i}(1) = hvar n(6) ; % Hardening variable (q)
      vartoplot{i}(2) = hvar_n(5) ; % Internal variable (r)
```

```
vartoplot{i}(3) = 1-hvar_n(6)/hvar_n(5) ; % Damage variable (d)
end
end
```

```
Error in damage_main (line 77)
E = Eprop(1) ; nu = Eprop(2) ;
```

```
function strain = calstrain NI(istep,STRAIN)
% See select_path
mstrain = size(STRAIN,2) ;
strain = zeros(sum(istep)+1,mstrain) ;
acum = 0 ;
PNT = STRAIN(1,:) ;
for iloc = 1:length(istep)
   INCSTRAIN = STRAIN(iloc+1,:)-STRAIN(iloc,:);
    for i = 1:istep(iloc)
        acum = acum + 1;
       PNTb = PNT ;
      % PNT = PNT+INCSTRAIN ;
      PNT = PNT + INCSTRAIN/istep(iloc);
       strain(acum+1,:) = PNT ;
    end
end
```

```
Error in calstrain_NI (line 3)
mstrain = size(STRAIN,2) ;
```