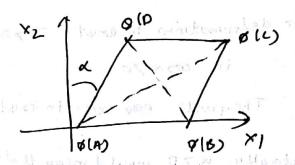
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## Computational solid Methanico

SH HWIB

Solution



Deformation mapping is terms of &

The deformation map is given by 
$$n = \emptyset(x/b) = \begin{bmatrix} x_1 + x_2 & y_1 \\ x_2 & y_2 \end{bmatrix}$$

as a the movement in x1 results in deformation in x1 but a movement along Ab worded be resolved in components.

compute the deprination gradient a right causely guen deformation two

$$f = \begin{bmatrix} \frac{\partial x_1}{\partial x_1} & \frac{\partial x_1}{\partial x_2} \\ \frac{\partial x_2}{\partial x_1} & \frac{\partial x_2}{\partial x_2} \end{bmatrix} = \begin{bmatrix} 1 & \sin x \\ 0 & \cos x \end{bmatrix}$$

$$C = PTF = \begin{bmatrix} 1 & 8ind \\ sind & 61 \end{bmatrix}$$

33) compute the variation is the volume of solid as a function of k dv = Jav where J = det(F) = cook

volumetre deformation +3(e) is denskel as e= dv-dV = J-1

aclmissible

for deformations to exist \$70

They will eas cease to exist when cos & < 0 or when a 7 1/2 geometrically, & 7 1/2 would mean that the diagonals lie or above A below the X1 axis. A In such a case the area is negotive.

The deformation may a greatly in a planty -

- change in the angle & subter ded by Hum. Interpret grometrically plot the change of leights and the change of angle & as a function of a.
- The length variation of diagonals be given by have & >BD

$$\lambda_{BD} = \left[ \begin{bmatrix} -1 & 1 \end{bmatrix} \begin{bmatrix} 1 & \sin x \\ \sin x & 1 \end{bmatrix} \begin{bmatrix} -1 \\ 1 \end{bmatrix} \right]$$

1 bor = 17 sind between a color outsimple subject of

The change in angle 12 is given by

$$E = \frac{1}{2}(C-I) = \frac{1}{2}\begin{bmatrix} 0 & \sin \alpha \\ \sin \alpha & 0 \end{bmatrix}$$

The denominators of eqn (1) are already computed in the previous section to be VI+sinx A VI-sinx

The numerator 13 given by

$$= \frac{1}{2} \left( -1 \pm \sin \lambda - \sin \alpha + 1 \right)$$

This is the original value of & : There is no charge in the argle even after deformation

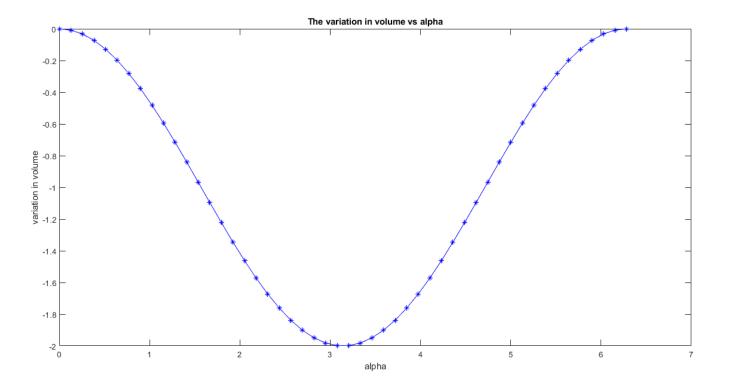
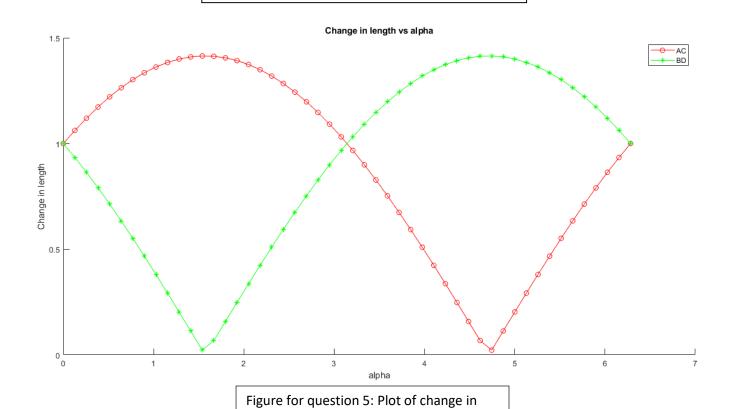


Fig for Q3: Plot of variation of Volume vs alpha



the length of diagonals vs alpha

$$\phi_1 = x^1$$
  $\phi_2 = x^2$   $\phi_3 = x^3 + \omega(x_1)x^2$ 

$$F = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ \frac{\partial w}{\partial x_1} & \frac{\partial w}{\partial x_2} \end{bmatrix}$$

$$C = f_{\perp} f_{\perp} = \begin{bmatrix} 1 + \left(\frac{9m}{9m}\right)_{2} & \frac{9m}{9m} \\ \frac{9m}{9m} & \frac{9m}{9m} & \frac{9m}{9m} \\ \frac{9m}{9m} & \frac{9m}{9m} & \frac{9m}{9m} \end{bmatrix}$$

816 Since the dat variation in volume is given by

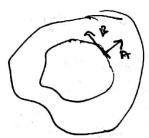
8= Jgo and J=1 the solid does not change volume

Since J>D, the Local impendicability conditions are satisfied

Q2 a we can see that  $A \cdot B = 0$  if  $A \in B$  must be perpendicular and in the same plane  $A = \frac{\nabla \cdot W}{||\nabla \cdot W||}$  if  $A = \frac{\nabla \cdot W}{||\nabla \cdot W||}$  is the unit normal vertor to the

outour a B must be the unit tangent vertor

The angle subtended by A & B & II



I a his brother some will

whi is simply written as we A who = W2

$$= \begin{bmatrix} \frac{\omega_1}{\sqrt{\omega_1^2 + \omega_2^2}} \\ \frac{\omega_2}{\sqrt{\omega_1^2 + \omega_2^2}} \\ \frac{\omega_1}{\sqrt{\omega_1^2 + \omega_2^2}} \\ \frac{\omega_1}{\sqrt{\omega_1^2 + \omega_2^2}} \\ \frac{\omega_1}{\sqrt{\omega_1^2 + \omega_2^2}} \\ \frac{\omega_1}{\sqrt{\omega_1^2 + \omega_2^2}} \\ \frac{\omega_2}{\sqrt{\omega_1^2 + \omega_2^2}} \\ \frac{\omega_1}{\sqrt{\omega_1^2 + \omega_2^2}} \\ \frac{\omega_1}{\sqrt{\omega_1^2 + \omega_2^2}} \\ \frac{\omega_2}{\sqrt{\omega_1^2 + \omega_2^2}} \\ \frac{\omega_2}{\sqrt{\omega_1^2$$

$$\lambda_{M^2} = \sqrt{\omega_1^2 + \omega_2^2 + 1} = \lambda_{M=1} \sqrt{\left(\frac{\partial \omega}{\partial x}\right)^2 + \frac{\partial \omega}{\partial x}} + 1$$

$$\lambda B^{2} = \begin{bmatrix} -w_{2} \\ \overline{v_{1}^{2} + w_{2}^{2}} \end{bmatrix} T \begin{bmatrix} 1 + w_{1}^{2} & w_{1}w_{2} & w_{1} \\ w_{1}w_{2} + w_{3}v_{1} \end{bmatrix} \begin{bmatrix} -w_{2} \\ \overline{v_{1}^{2} + w_{2}^{2}} \end{bmatrix} T \begin{bmatrix} 1 + w_{1}^{2} & w_{1}w_{2} & w_{1} \\ w_{1}w_{2} & w_{3}v_{4} \end{bmatrix} \begin{bmatrix} -w_{2} \\ \overline{v_{1}^{2} + w_{2}^{2}} \end{bmatrix} T \begin{bmatrix} 1 + w_{1}^{2} & w_{1}w_{2} & w_{1} \\ w_{1}w_{2} & w_{2} & w_{3}v_{4} \end{bmatrix} \begin{bmatrix} -w_{2} \\ \overline{v_{1}^{2} + w_{2}^{2}} \end{bmatrix} T \begin{bmatrix} 1 + w_{1}^{2} & w_{1}w_{2} & w_{1} \\ w_{1}w_{2} & w_{2} & w_{3}v_{4} \end{bmatrix} \begin{bmatrix} -w_{2} \\ \overline{v_{1}^{2} + w_{2}^{2}} \end{bmatrix} T \begin{bmatrix} 1 + w_{1}v_{1} & w_{1}w_{2} & w_{1} \\ w_{1}w_{2} & w_{2} & w_{3}v_{4} \end{bmatrix} \begin{bmatrix} -w_{2} \\ \overline{v_{1}^{2} + w_{2}^{2}} \end{bmatrix} T \begin{bmatrix} 1 + w_{1}v_{1} & w_{1}w_{2} & w_{1} \\ w_{1}w_{2} & w_{2} & w_{3}v_{4} \end{bmatrix} \begin{bmatrix} -w_{2} \\ \overline{v_{1}^{2} + w_{2}^{2}} \end{bmatrix} T \begin{bmatrix} 1 + w_{1}v_{1} & w_{1}w_{2} & w_{1} \\ w_{1}w_{2} & w_{2} & w_{3}v_{4} \end{bmatrix} T \begin{bmatrix} 1 + w_{1}v_{1} & w_{1}w_{2} & w_{1} \\ w_{1}w_{2} & w_{2} & w_{3}v_{4} \end{bmatrix} T \begin{bmatrix} 1 + w_{1}v_{1} & w_{1}w_{2} & w_{1} \\ w_{1}w_{2} & w_{2} & w_{3}v_{4} \end{bmatrix} T \begin{bmatrix} 1 + w_{1}v_{1} & w_{1}w_{2} & w_{1} \\ w_{1}w_{2} & w_{2} & w_{3}v_{4} \end{bmatrix} T \begin{bmatrix} 1 + w_{1}v_{1} & w_{1}w_{2} & w_{2} \\ w_{1}w_{2} & w_{3}v_{4} & w_{3}v_{4} \end{bmatrix} T \begin{bmatrix} 1 + w_{1}v_{1} & w_{1}w_{2} & w_{1}v_{4} \\ w_{2}v_{3} & w_{3}v_{4} & w_{3}v_{4} \end{bmatrix} T \begin{bmatrix} 1 + w_{1}v_{1} & w_{1}w_{2} & w_{1}v_{4} \\ w_{1}w_{2} & w_{1}v_{4} & w_{2}v_{4} \end{bmatrix} T \begin{bmatrix} 1 + w_{1}v_{1} & w_{1}w_{2} & w_{1}v_{4} \\ w_{1}w_{2} & w_{2}v_{4} & w_{1}v_{4} \end{bmatrix} T \begin{bmatrix} 1 + w_{1}v_{1} & w_{1}w_{2} & w_{1}v_{4} \\ w_{1}w_{2} & w_{2}v_{4} & w_{2}v_{4} \end{bmatrix} T \begin{bmatrix} 1 + w_{1}v_{1} & w_{1}v_{4} & w_{2}v_{4} \\ w_{1}w_{2} & w_{2}v_{4} & w_{2}v_{4} \end{bmatrix} T \begin{bmatrix} 1 + w_{1}v_{1} & w_{1}v_{4} & w_{2}v_{4} \\ w_{1}v_{2} & w_{2}v_{4} & w_{2}v_{4} \end{bmatrix} T \begin{bmatrix} 1 + w_{1}v_{1} & w_{1}v_{4} & w_{2}v_{4} \\ w_{1}v_{2} & w_{2}v_{4} & w_{2}v_{4} \end{bmatrix} T \begin{bmatrix} 1 + w_{1}v_{1} & w_{2}v_{4} & w_{2}v_{4} \\ w_{1}v_{2} & w_{2}v_{4} & w_{2}v_{4} \end{bmatrix} T \begin{bmatrix} 1 + w_{1}v_{1} & w_{1}v_{4} & w_{2}v_{4} \\ w_{1}v_{2} & w_{2}v_{4} & w_{2}v_{4} \end{bmatrix} T \begin{bmatrix} 1 + w_{1}v_{1} & w_{1}v_{4} & w_{2}v_{4} \\ w_{1}v_{2} & w_{2}v_{4} & w_{2}v_{4} \end{bmatrix} T \begin{bmatrix} 1 + w_{1}v_{1} & w_{1}v_{4} & w_{2}v_{4} \\ w_{1}v_{2} & w_{2}v_{4} & w_{2}v_{4} \end{bmatrix} T$$

The angle subtended is II

The vector & increases in size as the stretch ratio is positive

K greater than I but A the basis vector B remains of the

Same size.

The day of the continue of a .

Let ds be an infinitesimal area in the reference configuration A unit vector normal to such an area can be definied as [0 01]

ds = JFT ds according to the Nanson's Formula

i deni = 1.

$$F^{-T} = \begin{bmatrix} 0 & -\omega_1 \\ 0 & 1 & -\omega_2 \\ -6 & 6 & 1 \end{bmatrix}$$

95 Desire an integral expression for the deformed area of the

using the relation  $\Delta \mathcal{E}$ .  $\Delta s = \det(f) f^{-T} N ds$ 

To compute the deformed are a we get

here 
$$N = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$
 or  $C = \begin{bmatrix} 1 & 0 & -w_1 \\ 0 & 1 & -w_2 \\ -w_1 & -w_2 & w_1^2 + w_2^2 + 1 \end{bmatrix}$ 

.. The untigral expression reduces to

$$X^1 = X^1(S)$$
 A  $X^2 = X^2(S)$  0 \leq S \leq \( \text{is the ancluyth} \)

as 
$$\frac{x^{1}(s)}{ds}$$
.  $E_{1} + E_{2} \times \frac{x^{2}(s)}{ds}$  is the vector tangent to  $\partial \Omega$ 

The deformed length of the oure is given by

DL = 
$$\int_{0}^{e} \sqrt{\frac{d\eta^{2}+d\eta^{2}+d\eta^{2}+d\eta^{2}}{d\eta^{2}}} d\eta$$
 here is is the parameter

In this partial lar case it can be rewritten as the model to and prince

$$\Delta l = \int_{0}^{L} \sqrt{CA.\pi \left[ \frac{(dx^{1})^{2} + (dx^{2})^{2}}{ds} \right]^{2}} ds^{\frac{1}{2}} ds^{\frac{1}{2}}$$

$$G \qquad \begin{array}{c} X \\ A = \begin{bmatrix} x_1 \\ \overline{4s} \\ x_1 \\ \overline{ds} \\ 0 \end{bmatrix}$$

: CA.A = (1+w12) x12+ 2w1w2x1x2+ (1+w124) x12

20L= \[ \sqrt{(1+\wint)^2 x1^2 + 2\winz x1x2 + (+\winz) x2 \(\frac{\alpha x1}{as})^2 + \(\frac{\alpha x2}{ax})^2 - 1)} JAMES HOLD BY

Eq(D) is the integral expression for the perimeter of the boundary.

The demonstrates of equ (1) are observed amples wither

[] [ xm2 1] x [1 1] y-1

(1+ AND - AND E 1-) 1

This is the original value of P. . There is no things in the

roys, among they distinguishing