

DAMAGE MODELS

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Abstract. This document presents the implementation of rate independent and dependent continuum damage models using a Matlab code. First we run three different stress paths to evaluate the correctness of rate independent models. Then a parametric study of rate dependent model or visco-damage model. The results show a good coherence as expected.

1 INTRODUCTION

Continuum damage constitutive models simulate the behaviour of materials that have loss of stiffness and irreversible degradation. To understand and validate this theory is important to perform computational test simulations.

The primary objective of this study is the development and implementation of the code and algorithm of damage models using Matlab. First we will present rate independent models and compare some of the results between three different stress paths.

The second part of the study involves rate dependent models. We do a parametric study to verify the correctness of the implementation and assess the influence of different parameters as viscosity (η), strain rate and time-integration method.

2 RATE INDEPENDENT MODELS

The code analyses plane strain cases. Symmetric, non-symmetric tension-compression and tension-only damage models are included in the Matlab code.

The material properties employed in the analysis are shown in the table 1. We do not include the units of each parameter because we consider they are consistent between the inputs and the outputs. This parameter will be used in all the problems and in the case that they vary, the value used will be indicated.

In figure 1 shows the initial damage surfaces of the three rate independent models in the stress space. The value of σ_y controls the size of the surface and ν controls the shape. The other parameters control the evolution of the damage surface when the stress tends to be beyond the surface.

To assess the code, three stress paths are used and we observe the evolution of the outputs and results. The stress paths three increments as indicated:

Table 1: Material properties

Parameter	Value
E	20000
ν	0.3
σ_y	250
q_∞	2.5
H	0.5

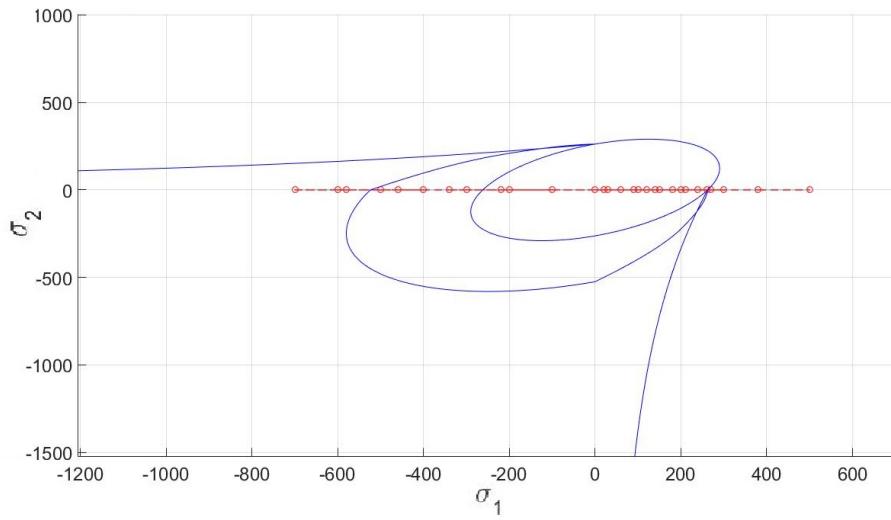


Figure 1: Initial damage surfaces in stress spaces.

1. Uniaxial stress path

$$\begin{aligned}\Delta\sigma_1^{(1)} &= 300 & ; \quad \Delta\sigma_2^{(1)} &= 0 \\ \Delta\sigma_1^{(2)} &= -1000 & ; \quad \Delta\sigma_2^{(2)} &= 0 \\ \Delta\sigma_1^{(3)} &= 1500 & ; \quad \Delta\sigma_2^{(3)} &= 0\end{aligned}$$

2. Uniaxial and biaxial stress path

$$\begin{aligned}\Delta\sigma_1^{(1)} &= 300 & ; \quad \Delta\sigma_2^{(1)} &= 0 \\ \Delta\sigma_1^{(2)} &= -1000 & ; \quad \Delta\sigma_2^{(2)} &= -1000 \\ \Delta\sigma_1^{(3)} &= 1500 & ; \quad \Delta\sigma_2^{(3)} &= 1500\end{aligned}$$

3. Biaxial stress path

$$\begin{aligned}\Delta\sigma_1^{(1)} &= 300 & ; \quad \Delta\sigma_2^{(1)} &= 300 \\ \Delta\sigma_1^{(2)} &= -1000 & ; \quad \Delta\sigma_2^{(2)} &= -1000 \\ \Delta\sigma_1^{(3)} &= 1500 & ; \quad \Delta\sigma_2^{(3)} &= 1500\end{aligned}$$

2.1 STRESS PATH 1

This problem consider uniaxial loading and unloading, for this reason we observe the evolution of stresses in direction 1 against the strain in direction 1 (see figures 2a, 3a and 4a). In figures 2b, 3b and 4b show the evolution of the hardening variable q .

We observe that in all the models the stress σ_1 do not goes further than 400 and q grows until reach the value of 2.5, because the parameter q_∞ limits the expansion of the damage surfaces. We observe that q is steady while the stress is inside the damage surface. For instance, in figure 3b, when σ_1 is in compression the value of q remains constant.

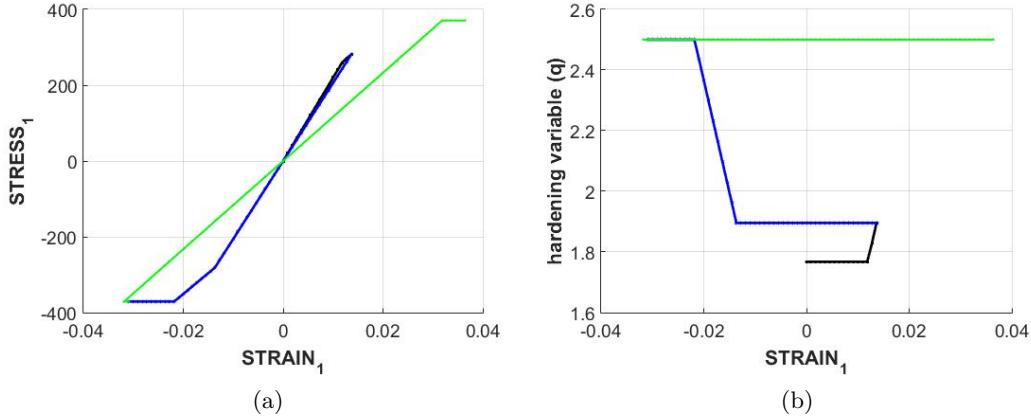


Figure 2: Symmetric damage model for case 1. (a) Principal major stress evolution. (b) Hardening variable evolution.

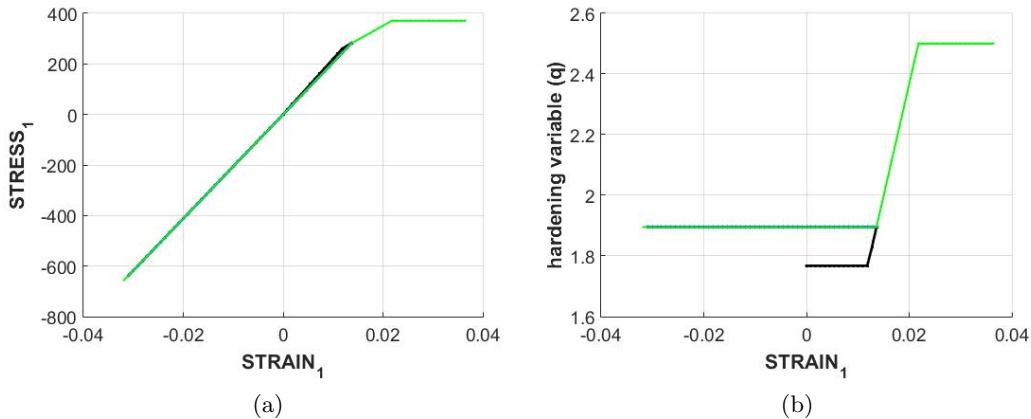


Figure 3: Only-tension damage model for case 1 (a) Principal major stress evolution. (b) Hardening variable evolution.

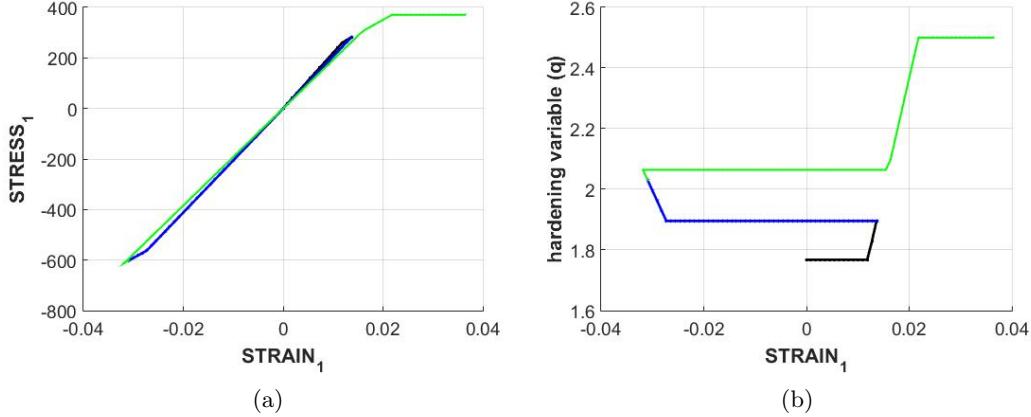


Figure 4: Non-symmetric tension-compression damage model for case 1. (a) Principal major stress evolution. (b) Hardening variable evolution.

Additionally, we compute the exponential hardening with the same parameters, except we added the parameter $A = 3$. The hardening modulus is not constant and his rate of change depends on A . Figure 5 shows the results of symmetric damage model with exponential hardening. We observe that in this model the value of q does not grow linearly and the evolution of σ_1 is not linear.

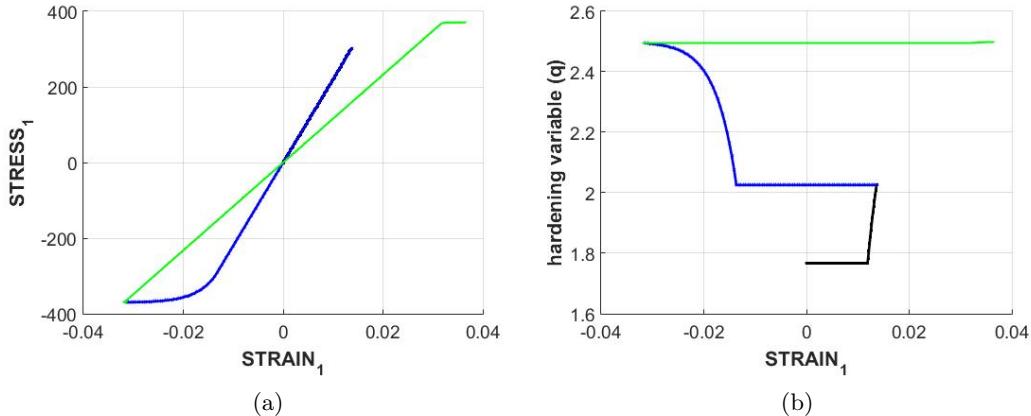


Figure 5: Symmetric damage model with exponential hardening for case 1. (a) Principal major stress evolution. (b) Hardening variable evolution.

2.2 STRESS PATH 2

This stress path considers a first tensile uniaxial load, afterwards the loading/unloading changes to biaxial. For this case we evaluate the stresses in 2-direction against the strains in 2-direction as shown figures 6b, 7b and 8.

We observe that in all cases there is a strain ε_2 and the stress σ_2 remains constant. This strain evolution is due to the poisson effect during the uniaxial tensile loading.

In figures 6b, 7b and 8 we plotted the evolution of the damage variable d . The value of d begin at 0 and increases when the stresses tend to be outside the elastic surface. This parameter evolves from 0 to 1. However, in this example as we restrict size of the damage surface with the parameter $q_\infty = 2.5$ and the value of d cannot reach 1.

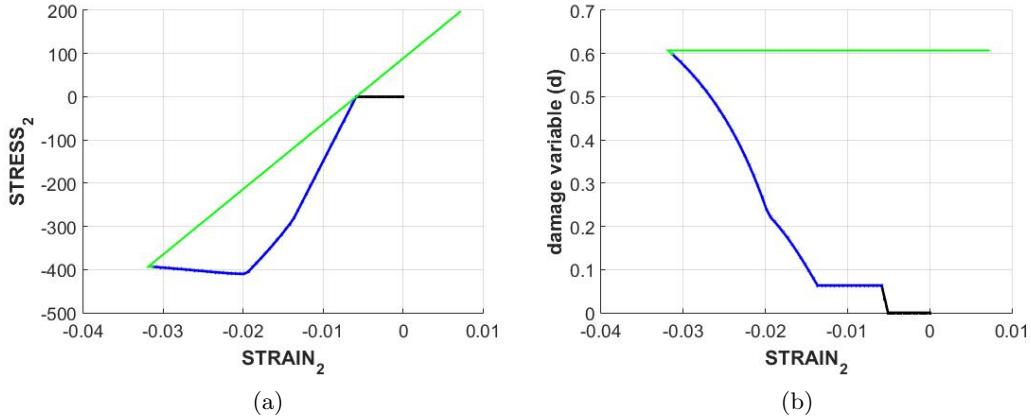


Figure 6: Symmetric damage model for case 2. (a) Principal major stress evolution. (b)Damage variable evolution.

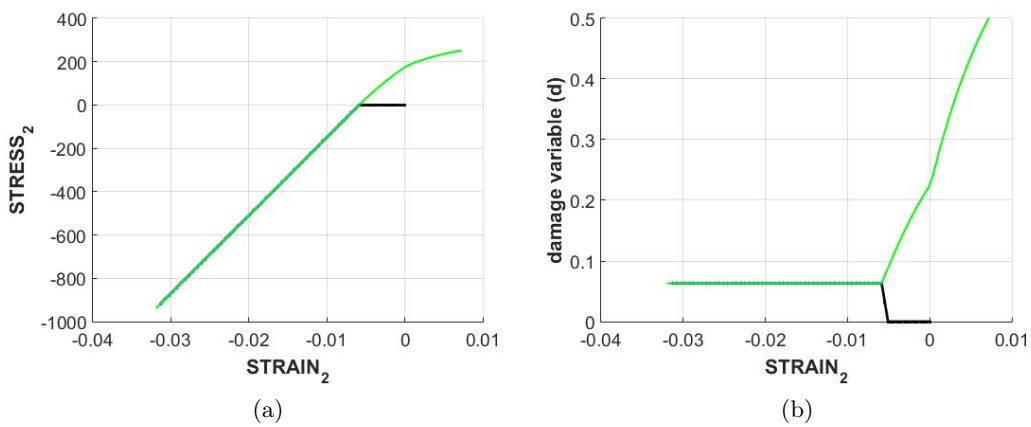


Figure 7: Only-tension damage model for case 2. (a) Principal major stress evolution. (b)Damage variable evolution.

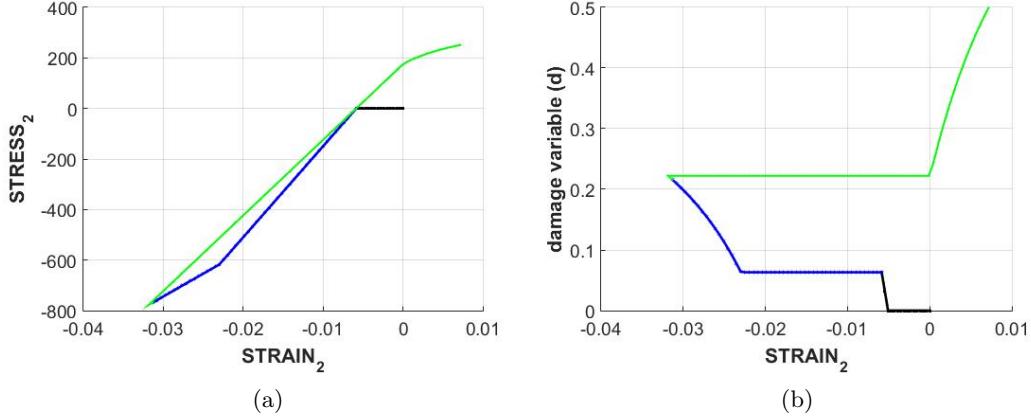


Figure 8: Non-symmetric tension-compression damage model for case 2 (a) Principal major stress evolution. (b) Damage variable evolution.

2.3 STRESS PATH 3

In this case we consider softening. To consider softening the value of H has to negative. In this example we change H to -0.2 and q_∞ to 0.5. Figures 9a, 10a and 11a show stress evolution against strain in 1-direction. The stress decrease after the damage surface is reached due to the the surface size decreases. Other way to observe the softening phenomenon is with that the hardening variable q decreases as shown figures 9b, 10b and 11b.

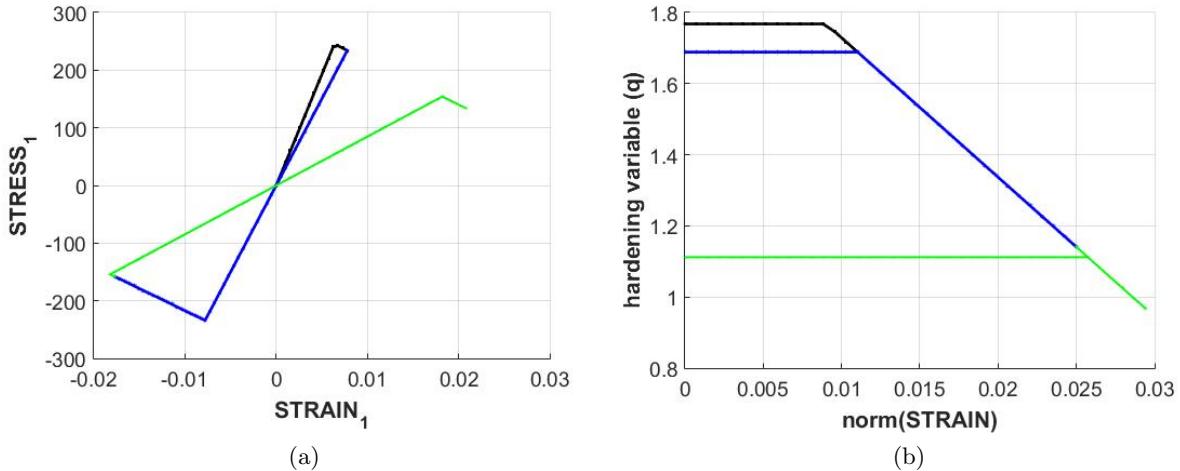


Figure 9: Symmetric damage model for case 3. (a) Principal major stress evolution. (b) Hardening variable evolution.

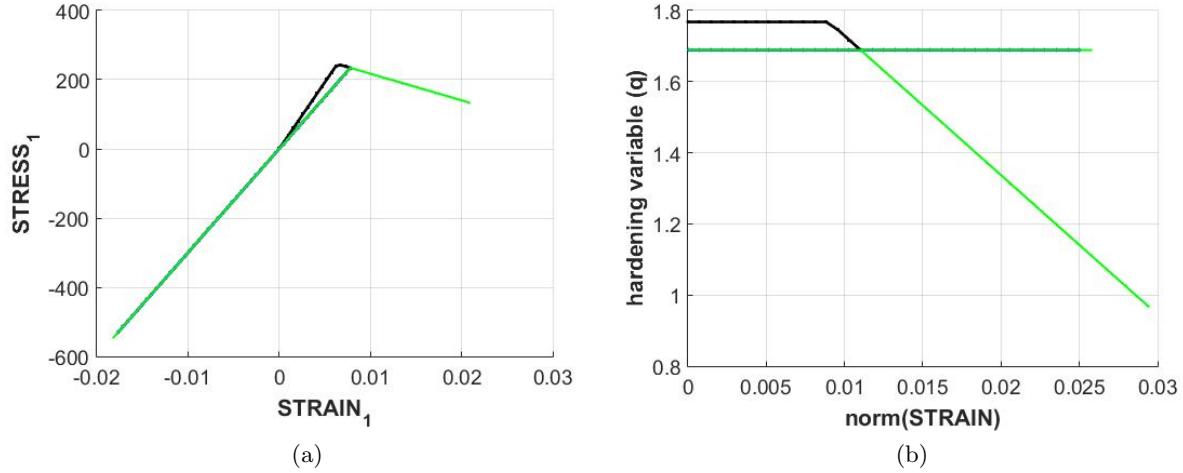


Figure 10: Only-tension damage model for case 3. (a) Principal major stress evolution. (b) Damage variable evolution.

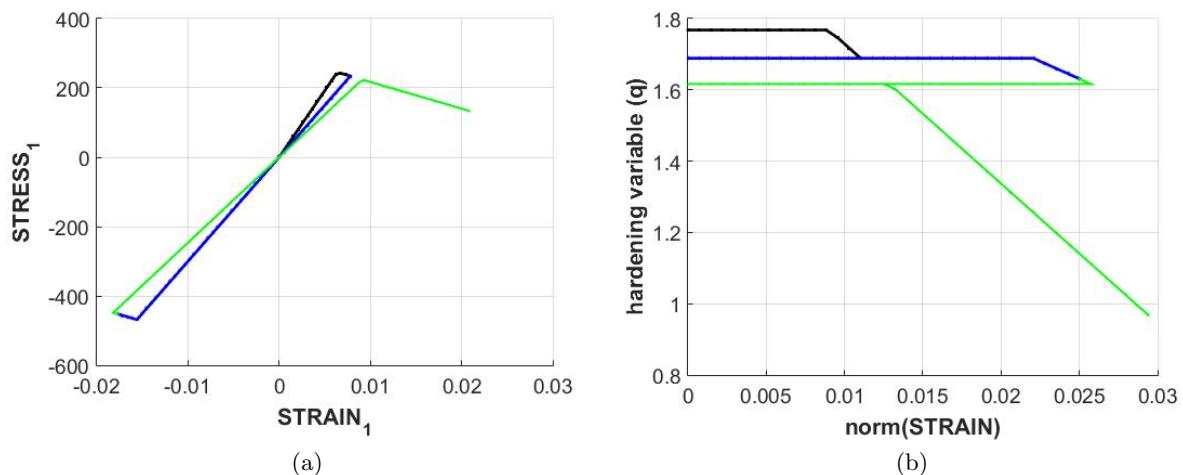


Figure 11: Non-symmetric tension-compression damage model for case 3. (a) Principal major stress evolution. (b) Damage variable evolution.

3 RATE DEPENDENT MODELS

Finally we implement in the Matlab code the integration algorithm for symmetric isotropic visco-damage model. The added a new function called `rmap_dano2.m`. The principal scripts of the code will be attached as an annex.

To do the parametric study we take as base the same parameters of the table 1 and additionally $\eta = 0.5$ and time of 10 s. The stress path to evaluate this model is uniaxial tensile loading to simplify the analysis.

1. Uniaxial stress path

$$\begin{aligned}\Delta\sigma_1^{(1)} &= 500 & ; \quad \Delta\sigma_2^{(1)} &= 0 \\ \Delta\sigma_1^{(2)} &= 500 & ; \quad \Delta\sigma_2^{(2)} &= 0 \\ \Delta\sigma_1^{(3)} &= 500 & ; \quad \Delta\sigma_2^{(3)} &= 0\end{aligned}$$

Figure 12 show the obtained stress-strain curves for different loading time (strain rate) and viscosity parameter η . As shows figure 12a, high strain rates higher stress σ_1 are reached. In figure 12b shows that high values of η reach higher values of stresses σ_1 .

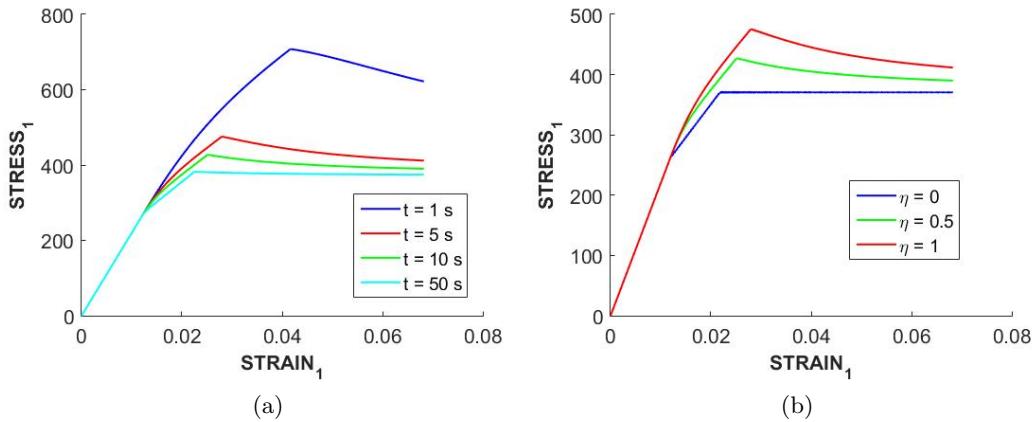


Figure 12: Initial damage surfaces in stress spaces.

In figure 13 shows the effect of α on time evolution of C_{11} component of the tangent and algorithmic constitutive operators. With a high number of time steps the solution with different values of α the result tend to be equal and the solution is more accurate. The differences is more visible with a smaller number of time steps as shown figure 13b. The value of C_{11} remains steady in the elastic range, then it increases slightly and falls significantly towards zero.

4 CONCLUSIONS

This work implemented the local constitutive response of continuum damage models. The results show good coherence. The evolution of hardening and damage variables (q and d) behaves as expected. For instance the value of d always grows when the stress state is or tend to be

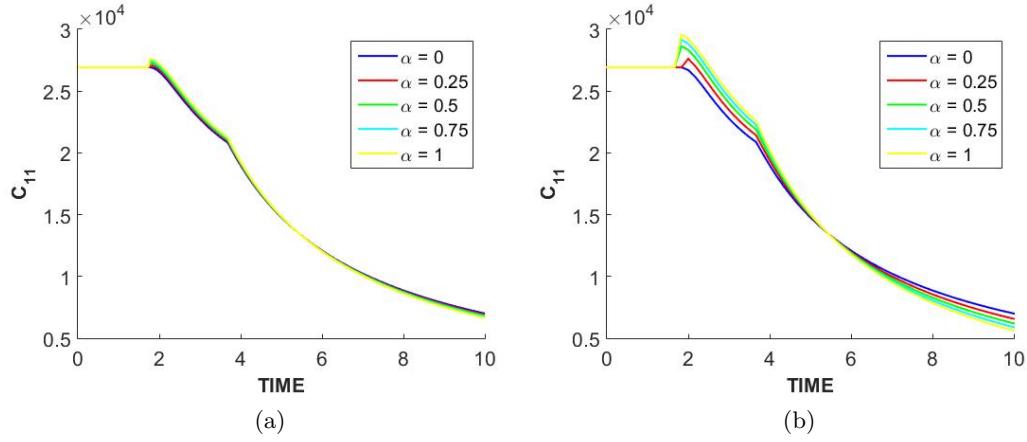


Figure 13: Evolution of C_{11} in time. (a) With 300 time steps. (b) With 30 time steps.

outside the elastic regime. The value of q increases on hardening behaviour and decreases on softening behaviour.

The model with exponential hardening was implemented successfully. This was confirmed with the evolution of hardening variable evolution and consequently the stress-strain curves.

The time steps has influence on the accuracy of rate dependent models.

5 ANNEX

```
1 clc
2 clear all
3 %%%%%%
4 % Program for modelling damage model
5 % (Elemental gauss point level)
6 % GRAPHIC INTERFACE
7 %
8 % Developed by J.Hdez Ortega
9 % 20-May-2007, Universidad PolitÃ©cnica de CataluÃ±a
10 %%%%%%
11 %profile on
12
13 % -----
14
15
16 current_dir = cd ;
17 if isunix
18     if exist('CALLBACK_main.m') == 2
19     else
20         addpath([current_dir, '/AUX_SUBROUTINES']);
21         % addpath(current_dir);
22     end
23
24     if exist('damage_main.m') == 2
25     else
26         addpath([current_dir]);
27         % addpath(current_dir);
28     end
29
30     pathdata = [current_dir, '/AUX_SUBROUTINES/WSFILES/'];
31
32 else
33     if exist('CALLBACK_main.m') == 2
34     else
35         addpath([current_dir, '\AUX_SUBROUTINES']);
36     end
37     if exist('damage_main.m') == 2
38     else
39         addpath([current_dir]);
40         % addpath(current_dir);
41     end
42     % addpath(current_dir);
43     pathdata = [current_dir, '\AUX_SUBROUTINES\WSFILES\'];
44 end
45
46 if exist(pathdata,'dir') == 0
47     mkdir( '\AUX_SUBROUTINES\WSFILES\' );
48 end
49
50
51 % ****
52 % INPUTS
53 % ****
54 %
55 % -----
```

```

56 % -----
57 Inc      = [0 -0.040 0 0] ;
58 NameFileExec = 'CALLBACK_main';
59 NameFileExecP = 'redraw_path';
60 Position = [0.01 0.9500 0.08 0.030] ;
61 PTC = {'SYMMETRIC','ONLY TENSION','NON-SYMMETRIC'} ;
62 TP = {'PLANE STRESS','PLANE STRAIN','3D'} ;
63 ce = 0 ;
64 nnls_s    = 3 ; % Number of load states
65 mstrain = 4 ; % Number of components of strain vector
66 mhist   = 6 ; % Number of components of historical variables vector
67 shownumber = 'YES' ;
68 axiskind   = 'NON-AUTO' ;
69 axislim    = [-500 500 -500 500] ;
70 ErasePrPlot = 'YES' ;
71 wplotx     ={'STRAIN_1','STRAIN_2','|STRAIN_1|','|STRAIN_2|','norm(STRAIN)', 'TIME'} ;
72 vpx        = 'STRAIN_1' ;
73 wploty     ={'STRESS_1','STRESS_2','|STRESS_1|','|STRESS_2|','norm(STRESS)'} ;
74 vpy        = 'STRESS_1' ;
75 splitwind  = 'YES' ;
76 HARDLIST   = {'LINEAR','EXPONENTIAL'} ;
77 % Inc      = [0 -0.040 0 0] ;
78 % -----
79 %Set of variables (to be stored in DATA)
80 % -----
81
82 % Workspace name
83 NameWs = [pathdata,'tmp1_maing.mat'];
84 %%%%%% MODEL INPUTS ( as uicontrols)
85 wplotx0 = wplotx;wploty0 = wploty;
86
87
88 COMPTA = 0 ;
89
90 if exist(NameWs) == 2
91     try
92         load(NameWs);
93     catch
94         COMPTA = 1 ;
95     end
96
97 else
98     COMPTA = 1 ;
99 end
100
101
102 if COMPTA == 1
103
104     % YOUNG's MODULUS
105     % -----
106     YOUNG_M = 20000 ;
107     % Poisson's coefficient
108     % -----
109     POISSON = 0.3 ;

```

```

110 % Hardening/softening modulus
111 % -----
112 HARDSOFT_MOD = -0.1 ;
113 % Yield stress
114 % -----
115 YIELD_STRESS = 200 ;
116 % Problem type TP = {'PLANE STRESS','PLANE STRAIN','3D'}
117 % -----
118 ntype_c = 'PLANE STRAIN' ;
119
120 % Number of increments of each load state
121 % -----
122 istep1 = 5 ;
123 istep2 = 6 ;
124 istep3 = 5 ;
125 % Ratio compression strength / tension strength
126 % -----
127 n = 3 ;
128 % Model PTC = {'SYMMETRIC','TRACTION','NON-SYMMETRIC'} ;
129 % -----
130 MDtype_c = 'SYMMETRIC' ;
131 try
132     save(NameWs) ;
133 catch
134     error('PATTERN PATH INCORRECT: Make sure that the current directory ↵
contains file main.m')
135 end
136 % SOFTENING/HARDENING TYPE
137 % -----
138 HARDTYPE = 'LINEAR' ; %{LINEAR,EXPONENTIAL}
139 % VISCOUS/INVISCID
140 % -----
141 VISCOUS = 'NO' ;
142 % Viscous coefficient ----
143 % -----
144 eta = 0.3 ;
145 % TimeTotal (initial = 0) ----
146 % -----
147 TimeTotal = 10 ;
148 % Integration coefficient ALPHA
149 % -----
150 ALPHA_COEFF = 0.5 ;
151     % Limit for q
152 % -----
153 q_inf = 2.5;
154 end
155 q_inf = 2.5;
156 A=0.5;
157
158
159 VARIABLES = {'YOUNG_M','POISSON','HARDSOFT_MOD','YIELD_STRESS','ntype_c', ...
160 'nnls_s','istep1','istep2','istep3','n','MDtype_c','mstrain', ...
161 'mhist','shownumber','axiskind','axislim','ErasePrPlot','vpx','vpy','splitwind','pathd ↵
ata', ...

```

```

162 %
163 % ****
164 % UICONTROLS
165 % ****
166 %
167
168 clf;figure(1);clf;
169 hold on
170 grid on
171 xlabel('\sigma_1','FontSize',24,'FontWeight','bold');
172 ylabel('\sigma_2','FontSize',24,'FontWeight','bold');
173 set(gca,'FontSize',18)
174 %-----
175 % Edit boxes  (-->VARIABLES_LEG), at the LEFT
176 %-----
177 VARIABLES_LEG = {'YOUNG_M','POISSON','HARDSOFT_MOD','YIELD_STRESS','q_inf','A'} ;
178 VARIABLES_TEXT = {'YOUNG_M','POISSON','HARDSOFT_MOD','YIELD_STRESS','q_inf','A'} ;
179 Inc_tv      = 0.002 ;
180 Inc_vt      = 0.002 ;
181 PositionT0 = [0.01 0.925 0.079 0.015] ;
182 PositionV0 = [0.01 0.9 0.079 0.023] ;
183 inclt = [ 0 PositionT0(4) + PositionV0(4) + Inc_tv + Inc_vt 0 0] ;
184 inclv = [0 PositionT0(4) + PositionV0(4) + Inc_vt + Inc_vt 0 0] ;
185 for ileg = 1:length(VARIABLES_LEG) ;
186     var_i = VARIABLES_LEG{ileg} ;      text_i = VARIABLES_TEXT{ileg} ;
187     if ~isempty(num2str(eval(var_i))); var_inum = num2str(eval(var_i)); else; %
var_inum = eval(var_i) ;    end
188     PositionT = PositionT0 - (ileg-1)*inclt;
189     STRE = ['htext = uicontrol(
(''Style'', ''text'', ''Units'', ''normalized'', ''Position'', ,
PositionT'', ''FontSize'', 9, ''string'', '''', text_i, '''); ];
190     eval(STRE);
191     PositionV = PositionV0 - (ileg-1)*inclv;
192     STRE =[ 'hp',num2str(ileg), ' = uicontrol(''Style'', ''edit'', ''String'', ,
var_inum, ''Units'', ''normalized'', ''Position'',PositionV'', ''FontSize'', 9, ''Tag'', '''', ,
var_i, '''', ''Callback'',NameFileExec); ];
193     eval(STRE);
194 end
195
196 % %%%%%%%%%%%%%%
197 % 2) MDtype_c
198 % %%%%%%%%%%%%%%
199 [ok MDtype] = FndStrInCell(PTC,MDtype_c) ;
200 fff =uicontrol('Style', 'text', 'String', 'Damage model',...
201     'Units','normalized','Position', [0.768 0.974 0.18 0.02], 'FontSize',
202     10, 'FontWeight','Bold');
203 fff =uicontrol('Style', 'popupmenu', 'String', PTC, ...
204     'Units','normalized','Position', [0.768 0.917 0.18 0.057], 'Callback',
205     NameFileExec, ...
206     'Tag','MDtype','Value',MDtype);
207
208 % %%%%%%%%%%%%%%
209 % 3) PROBLEM TYPE --> TP
210 % %%%%%%%%%%%%%%

```

```

209 [ok ntype] = FndStrInCell(TP,ntype_c) ;
210 fff =uicontrol('Style', 'text', 'String', 'Problem type',...
211     'Units','normalized','Position', [0.568 0.974 0.18 0.02], 'FontSize', \
212     'FontWeight','Bold');
213 fff =uicontrol('Style', 'popupmenu', 'String', TP, ...
214     'Units','normalized','Position', [0.568 0.917 0.18 0.057], 'Callback', \
NameFileExec,...,
215     'Tag','ntype_c','Value',ntype);
216 % %%%%%%%%%%%%%%%%
217 % 4) Ratio compression/traction strength
218 fff =uicontrol('Style', 'text', 'String', {'ONLY FOR ','NON-`', \
SYMMETRIC','-----'},...
219     'Units','normalized','Position',[0.01 0.435 0.08 0.050], 'FontSize', \
9,'FontWeight','Bold');
220 fff =uicontrol('Style', 'text', 'String', 'ratio comp/trac',...
221     'Units','normalized','Position',[0.01 0.42 0.08 \
0.02], 'FontWeight','Bold','FontSize',9);
222 fff =uicontrol('Style', 'edit', 'String', num2str(n),...
223     'Units','normalized','Position',[0.01 0.4 0.08 0.02], 'FontSize', \
9,'tag','n',...
224     'Callback',NameFileExec);
225 % %%%%%%%%%%%%%%%%
226 % 5) INCREMENTS FOR EACH LOAD STATE
227 % %%%%%%%%%%%%%%%%
228 fff =uicontrol('Style', 'text', 'String', {'INCREMENTS','-----'},...
229     'Units','normalized','Position',[0.913 0.893 0.08 0.030], 'FontSize', \
9,'FontWeight','Bold');
230 VARIABLES_LEG2 = {'istep1','istep2','istep3'};
231 Position = [0.913 0.893 0.08 0.025];
232 Inc      = [0 -0.030 0 0];
233
234 for ileg = 1:length(VARIABLES_LEG2)
235     var_i = VARIABLES_LEG2{ileg};
236     var_inum = num2str(eval(var_i));
237     Position = Position + Inc;
238     STRE = ['htext = uicontrol' \
(''Style'', ''text'', 'Units', 'normalized', 'Position', Position, 'FontSize', \
9, 'string', '', var_i, '');'];
239     eval(STRE);
240     Position = Position + Inc;
241     STRE =[ 'hp', num2str(ileg), ' = uicontrol(''Style'', 'edit', 'String', \
var_inum, 'Units', 'normalized', 'Position', Position, 'FontSize', 9, 'Tag', '', \
var_i, '', 'Callback', NameFileExecP); ];
242     eval(STRE);
243 end
244
245 % -----
246 % Pushbottoms
247 % -----
248 hpushsell = uicontrol('Style','pushbutton',...
249     'String',{'SELECT LOAD PATH'}, 'Units', 'normalized', 'Position', [0.006 0.119 \
0.08 0.0336], 'Callback', 'select_path', ...
250     'tag','select_load');
251

```

```

252 hpushsell = uicontrol('Style','pushbutton',...
253     'String',{'COMPUTE'},'Units','normalized','Position',[0.006 0.065 0.08↖
0.044], 'Callback','compute_load', ...
254     'tag','c');
255
256 hpushsell = uicontrol('Style','pushbutton',...
257     'String',{'REFRESH'},'Units','normalized','Position',[0.006 0.022 0.08↖
0.03687], 'Callback','refresh_main', ...
258     'tag','c');
259
260 hpushsell = uicontrol('Style','pushbutton',...
261     'String',{'OPTIONS'},'Units','normalized','Position',[0.1 0.94 0.08↖
0.05], 'Callback','showoptions', ...
262     'tag','showoptions2');
263
264
265 % %%%%%%%%%%%%%%
266 % *) PLOT X
267 % %%%%%%%%%%%%%%
268 [ok nvx] = FndStrInCell(wplotx,vpx) ;
269 fff =uicontrol('Style', 'text', 'String', 'VAR X',...
270     'Units','normalized','Position', [0.2 0.974 0.14 0.02], 'FontSize',↖
10,'FontWeight','Bold');
271 fff =uicontrol('Style', 'popupmenu', 'String', wplotx,...
272     'Units','normalized','Position', [0.2 0.917 0.14↖
0.057], 'Callback','plotcurves',...
273     'Tag','xplotc','Value',nvx);
274 % %%%%%%%%%%%%%%
275 % *) PLOT Y
276 % %%%%%%%%%%%%%%
277 [ok nvy] = FndStrInCell(wploty,vpy) ;
278 fff =uicontrol('Style', 'text', 'String', 'VAR Y',...
279     'Units','normalized','Position', [0.36 0.974 0.14 0.02], 'FontSize',↖
10,'FontWeight','Bold');
280 fff =uicontrol('Style', 'popupmenu', 'String', wploty,...
281     'Units','normalized','Position', [0.36 0.917 0.14↖
0.057], 'Callback','plotcurves',...
282     'Tag','yplotc','Value',nvy);
283
284 %%% HARDTYPE
285 [ok ntype] = FndStrInCell(HARDLIST,HARDTYPE) ;
286 fff =uicontrol('Style', 'text', 'String', 'HARD/SOFT EV.',...
287     'Units','normalized','Position',[0.01 0.665 0.079 0.015] , 'FontSize',↖
9,'FontWeight','Bold');
288 fff =uicontrol('Style', 'popupmenu', 'String', HARDLIST,...
289     'Units','normalized','Position',[0.01 0.64 0.077 0.023] , 'Callback',↖
NameFileExec,...
290     'Tag','HARDTYPE_tag','Value',ntype,'FontSize',8);
291
292 %%% VISCOSUS
293 [ok ntype] = FndStrInCell({'YES','NO'},VISCOSUS) ;
294 fff =uicontrol('Style', 'text', 'String', 'VISCOSUS MODEL',...
295     'Units','normalized','Position',[0.01 0.615 0.079 0.015] , 'FontSize',↖
9,'FontWeight','Bold');
296 fff =uicontrol('Style', 'popupmenu', 'String',{ 'YES','NO'} , ...

```

```

297     'Units','normalized','Position',[0.01 0.59 0.077 0.023] , 'Callback', ↵
NameFileExec, ...
298     'Tag','VISCOSUS_tag','Value',ntype,'FontSize',8);
299
300 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
301
302 %-----%
303 % Edit boxes OTHER PARAMETERS
304 %-----%
305 VARIABLES_LEG3 = {'eta','TimeTotal','ALPHA_COEFF'};
306 VARIABLES_TEXT = {'viscous coeff.', 'TIME INT.(s)', 'ALPHA coeff.'};
307 Inc_tv      = 0.004 ;
308 Inc_vt      = 0.004 ;
309 PositionT0 = [0.913 0.66 0.08 0.025 ] ; %0.01 0.61 0.079 0.015 0.913 0.893 0.08 ↵
0.025
310 PositionV0 = [0.913 0.645 0.08 0.025 ] ; %0.01 0.865 0.079 0.023
311 inclt = [ 0 PositionT0(4) + PositionV0(4) + Inc_tv + Inc_vt 0 0] ;
312 inclv = [0 PositionT0(4) + PositionV0(4) + Inc_vt + Inc_vt 0 0] ;
313 for ileg = 1:length(VARIABLES_LEG3) ;
314     var_i = VARIABLES_LEG3{ileg} ;      text_i = VARIABLES_TEXT{ileg} ;
315     if ~isempty(num2str(eval(var_i))); var_inum = num2str(eval(var_i)); else; ↵
var_inum = eval(var_i) ;    end
316     PositionT = PositionT0 - (ileg-1)*inclt;
317     STRE = ['htext = uicontrol' ↵
(''Style'', ''text'', ''Units'', ''normalized'', ''Position'', ↵
PositionT'', ''FontWeight'', ''Bold'', ''FontSize'', 9, ''string'', '''', text_i, '''');'] ;
318     eval(STRE);
319     PositionV = PositionV0 - (ileg-1)*inclv;
320     STRE =[ 'hp',num2str(ileg), ' = uicontrol(''Style'', ''edit'', ''String'', ↵
var_inum,''Units'', ''normalized'', ''Position'',PositionV'', ''FontSize'', 9, ''Tag'', '''', ↵
var_i, '''', ''Callback'',NameFileExec);'];
321     eval(STRE);
322 end
323
324
325
326 %*****%
327 % Storing all variables in DATA
328 %*****%
329 for ivar = 1:length(VARIABLES) ;
330     num_var = VARIABLES{ivar};
331     eval(['DATA.VAR.',num_var,' = ',num_var,';']);
332 end
333 DATA.VARIABLES_LEG = VARIABLES_LEG ;
334 DATA.VARIABLES_LEG2 = VARIABLES_LEG2 ;
335 DATA.VARIABLES_LEG3 = VARIABLES_LEG3 ;
336 DATA.NameWs        = NameWs        ;
337 DATA.wplotx0 = wplotx0 ;
338 DATA.wploty0 = wploty0 ;
339
340 %-----%
341 % Attach DATA to the current figure
342 %-----%
343 guidata(gcf,DATA);
344 CALLBACK_main      ;

```

```
345
346
347 %profile report
348
```



```

51 % 1) sigma_v{itime}(icomp,jcomp) --> Component (icomp,jcomp) of the cauchy
52 % stress tensor at step "itime"
53 % REMARK: sigma_v is a type of
54 % variable called "cell array".
55 %
56 %
57 % 2) vartoplot{itime} --> Cell array containing variables one wishes ↵
to plot
58 %
59 % vartoplot{itime}(1) = Hardening variable (q)
60 % vartoplot{itime}(2) = Internal variable (r)%
61 %
62 %
63 % 3) LABELPLOT{ivar} --> Cell array with the label string for
64 % variables of "varplot"
65 %
66 % LABELPLOT{1} => 'hardening variable (q)'
67 % LABELPLOT{2} => 'internal variable'
68 %
69 %
70 % 4) TIME VECTOR - >
71 %
%%%%%%%%%%%%%%%
72
73 % SET LABEL OF "vartoplot" variables (it may be defined also outside this ↵
function)
74 %
75 LABELPLOT = {'hardening variable (q)', 'internal variable'};
76 LABELPLOT{3} = 'damage variable (d)';
77 LABELPLOT{4} = 'C11';
78
79 E = Eprop(1); nu = Eprop(2);
80 viscpr = Eprop(6);
81 sigma_u = Eprop(4);
82
83
84
85 if ntype == 1
86     menu('PLANE STRESS has not been implemented yet', 'STOP');
87     error('OPTION NOT AVAILABLE')
88     mstrain = 4;
89     mhyst = 6;
90 elseif ntype == 3
91     menu('3-DIMENSIONAL PROBLEM has not been implemented yet', 'STOP');
92     error('OPTION NOT AVAILABLE')
93 else
94     mstrain = 4;
95     mhyst = 6;
96 end
97
98 totalstep = sum(istep);
99
100
101 % INITIALIZING GLOBAL CELL ARRAYS

```

```

102 % -----
103 sigma_v = cell(totalstep+1,1) ;
104 TIMEVECTOR = zeros(totalstep+1,1) ;
105 delta_t = TimeTotal./istep/length(istep) ;
106
107
108 % Elastic constitutive tensor
109 % -----
110 [ce] = tensor_elasticol (Eprop, ntype);
111 % Init.
112 % -----
113 % Strain vector
114 % -----
115 eps_n1 = zeros(mstrain,1);
116 % Historic variables
117 % hvar_n(1:4) --> empty
118 % hvar_n(5) = q --> Hardening variable
119 % hvar_n(6) = r --> Internal variable
120 hvar_n = zeros(mhist,1) ;
121
122 % INITIALIZING (i = 1) !!!!*
123 % ****i*
124 i = 1 ;
125 r0 = sigma_u/sqrt(E);
126 hvar_n(5) = r0; % r_n
127 hvar_n(6) = r0; % q_n
128 eps_n1 = strain(i,:) ;
129 sigma_n1 = ce*eps_n1'; % Elastic
130 sigma_v{i} = [sigma_n1(1) sigma_n1(3) 0; sigma_n1(3) sigma_n1(2) 0 ; 0 0 sigma_n1(4)];
131
132 nplot = 3 ;
133 vartoplot = cell(1,totalstep+1) ;
134 vartoplot{i}(1) = hvar_n(6) ; % Hardening variable (q)
135 vartoplot{i}(2) = hvar_n(5) ; % Internal variable (r)
136 vartoplot{i}(3) = 1-hvar_n(6)/hvar_n(5) ; % Damage variable (d)
137 vartoplot{i}(4) = ce(1,1) ; % C11 (d)
138
139 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
140 %*****%
141 % INVISCID
142 % *****%
143
144 if viscpr == 0
145 for iload = 1:length(istep)
146     % Load states
147     for iloc = 1:istep(iload)
148         i = i + 1 ;
149         TIMEVECTOR(i) = TIMEVECTOR(i-1)+ delta_t(iload) ;
150         % Total strain at step "i"
151         % -----
152         eps_n1 = strain(i,:) ;
153         %*
154         %*      DAMAGE MODEL

```

```

155 % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % %
156 [sigma_n1,hvar_n,aux_var] = rmap_dano1(eps_n1,hvar_n,Eprop,ce,MDtype,n);
157 % PLOTTING DAMAGE SURFACE
158 if(aux_var(1)>0)
159     hplotSURF(i) = dibujar_criterio_dano1(ce, nu, hvar_n(6), 'r:',MDtype,n)
160 );
161     set(hplotSURF(i), 'Color',[0 0 1], 'LineWidth',1)
162 ;
163 end
164 %*****%
165 % GLOBAL VARIABLES
166 % *****
167 % Stress
168 % -----
169 m_sigma=[sigma_n1(1) sigma_n1(3) 0;sigma_n1(3) sigma_n1(2) 0 ; 0 0
sigma_n1(4)];
170 sigma_v{i} = m_sigma ;
171
172 % VARIABLES TO PLOT (set label on cell array LABELPLOT)
173 % -----
174 vartoplot{i}(1) = hvar_n(6); % Hardening variable (q)
175 vartoplot{i}(2) = hvar_n(5); % Internal variable (r)
176 vartoplot{i}(3) = 1-hvar_n(6)/hvar_n(5); % Damage variable (d)
177 vartoplot{i}(4) = aux_var(4); % C11 (d)
178
179 end
180 end
181 %*****%
182 %*****%
183 % VISCOSUS
184 % *****
185
186 else
187 for iload = 1:length(istep)
188 % Load states
189 for iloc = 1:istep(iload)
190 i = i + 1;
191 TIMEVECTOR(i) = TIMEVECTOR(i-1)+ delta_t(iload);
192 % Total strain at step "i"
193 % -----
194 timestep=TIMEVECTOR(i)-TIMEVECTOR(i-1);
195 eps_n = strain(i-1,:);
196 eps_n1 = strain(i,:);
197 % *
*****%
198 %* DAMAGE MODEL
199 % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % %
200 [sigma_n1,hvar_n,aux_var] = rmap_dano2(eps_n,eps_n1,hvar_n,Eprop,ce,
MDtype,n,timestep);
201 % PLOTTING DAMAGE SURFACE
202 if(aux_var(1)>0)
203     hplotSURF(i) = dibujar_criterio_dano1(ce, nu, hvar_n(6), 'r:',MDtype,n)
204 );

```

```
204         set(hplotSURF(i), 'Color',[0 0 1], 'LineWidth',1) ↵
;
205     end
206
207 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
208 %*****GLOBAL VARIABLES*****
209 % Stress
210 % -----
211 %_sigma=[sigma_n1(1) sigma_n1(3) 0;sigma_n1(3) sigma_n1(2) 0 ; 0 0 ↵
sigma_n1(4)];
212         sigma_v{i} = _sigma ;
213
214
215 % VARIABLES TO PLOT (set label on cell array LABELPLOT)
216 % -----
217 vartoplot{i}(1) = hvar_n(6) ; % Hardening variable (q)
218 vartoplot{i}(2) = hvar_n(5) ; % Internal variable (r)
219 vartoplot{i}(3) = 1-hvar_n(6)/hvar_n(5) ; % Damage variable (d)
220 vartoplot{i}(4) = aux_var(4) ; % C11 (d)
221
222
223 end
224 end
225 end
226
```

```

1 function [sigma_n1,hvar_n1,aux_var] = rmap_dano1 (eps_n1,hvar_n,Eprop,ce,MDtype,n)
2
3 %*
4 %*                                         *
5 %*          Integration Algorithm for a isotropic damage model
6 %*
7 %* *
8 %*          [sigma_n1,hvar_n1,aux_var] = rmap_dano1 (eps_n1,hvar_n,Eprop,ce) *
9 %* *
10 %* INPUTS           eps_n1(4)    strain (almansi)    step n+1*
11 %*                   vector R4    (exx eyy exy ezz)*
12 %*                   hvar_n(6)   internal variables , step n*
13 %*                   hvar_n(1:4) (empty) *
14 %*                   hvar_n(5) = r ; hvar_n(6)=q*
15 %*                   Eprop(:)   Material parameters*
16 %*
17 %*                   ce(4,4)    Constitutive elastic tensor*
18 %* *
19 %* OUTPUTS:        sigma_n1(4) Cauchy stress , step n+1*
20 %*                   hvar_n(6)   Internal variables , step n+1*
21 %*                   aux_var(3) Auxiliar variables for computing const. tangent*
tensor  *
22 %*
*****                                         * *
23
24
25 hvar_n1 = hvar_n;
26 r_n      = hvar_n(5);
27 q_n      = hvar_n(6);
28 E        = Eprop(1);
29 nu       = Eprop(2);
30 H        = Eprop(3);
31 sigma_u = Eprop(4);
32 hard_type = Eprop(5);
33 viscpr = Eprop(6);
34 eta = Eprop(7);
35 alpha = Eprop(8);
36 q_inf = Eprop(9);
37 A = Eprop(10);
38
39 %

```

```

*****
40
41
42 % ↵
*****
43 %*      initializing
44 r0 = sigma_u/sqrt(E);
45 zero_q=1.d-6*r0;
46 % if(r_n<=0.d0)
47 %   r_n=r0;
48 %   q_n=r0;
49 % end
50 % ↵
*****
51
52
53 % ↵
*****
54 %*      Damage surface ↵
%*
55 [rtrial] = Modelos_de_dano1 (MDtype,ce,eps_n1,n);
56 % ↵
*****
57
58
59 % ↵
*****
60 %*      Ver el Estado de Carga ↵
%*
61 %*      -----> fload=0 : elastic unload ↵
%*
62 %*      -----> fload=1 : damage (compute algorithmic constitutive tensor) ↵
%*
63 fload=0;
64
65 if(rtrial > r_n)
66   %* Loading
67
68   fload=1;
69   delta_r=rtrial-r_n;
70   r_nl= rtrial ;
71   if hard_type == 0
72     % Linear
73     q_nl= min(q_n+ H*delta_r , q_inf);
74   else
75     % Exponential
76     q_nl= q_inf-(q_inf-r0)*exp(A*(1-r_nl/r0));
77     H=A*(q_inf-r0)*exp(A*(1-r_nl/r0))/r0;
78   end
79
80   if(q_nl<zero_q)
81     q_nl=zero_q;
82   end
83   s_n1 =ce*eps_n1';
84   ce_nl=s_n1*s_nl';

```

```

85      c11_n1=ce(1,1)*q_n1/r_n1-(q_n1-H*r_n1)/r_n1^3*ce_n1(1,1);
86
87 else
88
89     %*      Elastic load/unload
90     fload=0;
91     r_n1= r_n ;
92     q_n1= q_n ;
93     c11_n1=ce(1,1)*q_n1/r_n1;
94
95
96 end
97 % Damage variable
98 % -----
99 dano_n1 = 1.d0-(q_n1/r_n1);
100 % Computing stress
101 % ****
102 sigma_n1 =(1.d0-dano_n1)*ce*eps_n1';
103 %hold on
104 %plot(sigma_n1(1),sigma_n1(2),'bx')
105
106 %*
*****  

107
108
109 %*
*****  

110 %* Updating historic variables          %*
111 % hvar_n1(1:4) = eps_nlp;
112 hvar_n1(5)= r_n1 ;
113 hvar_n1(6)= q_n1 ;
114 %*
*****  

115
116
117 %*
*****  

118 %* Auxiliar variables  

%*
119 aux_var(1) = fload;
120 aux_var(2) = q_n1/r_n1;
121 aux_var(3) = (q_n1-H*r_n1)/r_n1^3;
122 aux_var(4) = c11_n1;
123 %*
*****  

124
125
126
127
128
129
130
131
132
133

```

134

135

```

1 function [sigma_n1,hvar_n1,aux_var] = rmap_dano2 (eps_n,eps_n1,hvar_n,Eprop,ce, \
MDtype,n,timestep)
2
3 %*
4 %* *
5 %* Integration Algorithm for a isotropic damage model
6 %*
7 %* *
8 %* [sigma_n1,hvar_n1,aux_var] = rmap_dano2 (eps_n,eps_n1,hvar_n,Eprop,ce,MDtype,n, \
timestep)*
9 %* *
10 %* INPUTS           eps_n1(4)    strain (almansi)    step n+1*
11 %*                   vector R4    (exx eyy exy ezz)*
12 %*                   hvar_n(6)   internal variables , step n*
13 %*                   hvar_n(1:4) (empty)*
14 %*                   hvar_n(5) = r ; hvar_n(6)=q*
15 %*                   Eprop(:)   Material parameters*
16 %*                   ce(4,4)   Constitutive elastic tensor*
17 %* *
18 %* *
19 %* OUTPUTS:        sigma_n1(4) Cauchy stress , step n+1*
20 %*                   hvar_n(6)   Internal variables , step n+1*
21 %*                   aux_var(3) Auxiliar variables for computing const. tangent*
tensor   *
22 %*
***** *
23
24
25 hvar_n1 = hvar_n;
26 r_n      = hvar_n(5);
27 q_n      = hvar_n(6);
28 E        = Eprop(1);
29 nu       = Eprop(2);
30 H        = Eprop(3);
31 sigma_u = Eprop(4);
32 hard_type = Eprop(5);
33 viscpr = Eprop(6);
34 eta = Eprop(7);
35 alpha = Eprop(8);
36 q_inf = Eprop(9);
37 A = Eprop(10);

```

```

38
39 % ↵
*****
40
41
42 % ↵
*****
43 %*      initializing          %
44 r0 = sigma_u/sqrt(E);
45 zero_q=1.d-6*r0;
46 % if(r_n<=0.d0)
47 %     r_n=r0;
48 %     q_n=r0;
49 % end
50 % ↵
*****
51
52
53 % ↵
*****
54 %*      Damage surface ↵
%*
55 [rtrial] = (1-alpha)*Modelos_de_danol (MDtype,ce,eps_n,n)+alpha*Modelos_de_danol ↵
(MDtype,ce,eps_n1,n);
56 [rtrialexp] = Modelos_de_danol (MDtype,ce,eps_n1,n);
57 [rtrialimp] = Modelos_de_danol (MDtype,ce,eps_n,n);
58 % ↵
*****
59
60
61 % ↵
*****
62 %*      Ver el Estado de Carga ↵
%*
63 %*      ----->      fload=0 : elastic unload ↵
%*
64 %*      ----->      fload=1 : damage (compute algorithmic constitutive tensor) ↵
%*
65 fload=0;
66
67 if(rtrial > r_n)
68     %*    Loading
69
70     fload=1;
71     r_n1= (eta-timestep*(1-alpha))*r_n/(eta+alpha*timestep)+timestep*rtrial/ ↵
(eta+alpha*timestep) ;
72     delta_r=r_n1-r_n;
73     if hard_type == 0
74         % Linear
75         q_n1= min(q_n+ H*delta_r , q_inf);
76     else
77         % Exponential
78         q_n1= q_inf-(q_inf-r0)*exp(A*(1-r_n1/r0));
79         H=A*(q_inf-r0)*exp(A*(1-r_n1/r0))/r0;
80

```

```

81     end
82
83     if(q_n1<zero_q)
84         q_n1=zero_q;
85     end
86     s_n1 =ce*eps_n1';
87     ce_n1=s_n1*s_n1';
88     c11_n1=ce(1,1)*q_n1/r_n1-alpha*timestep*(H*r_n1-q_n1)/((eta+alpha*timestep) ↵
*rttrial*r_n1^2)*ce_n1(1,1);
89
90 else
91
92     %*      Elastic load/unload
93     fload=0;
94     r_n1= r_n ;
95     q_n1= q_n ;
96     c11_n1=ce(1,1)*q_n1/r_n1;
97
98 end
99 % Damage variable
100 % -----
101 dano_n1 = 1.d0-(q_n1/r_n1);
102 % Computing stress
103 % ****
104 sigma_n1 =(1.d0-dano_n1)*ce*eps_n1';
105 %hold on
106 %plot(sigma_n1(1),sigma_n1(2),'bx')
107
108 %*
*****  

109
110
111 %*
*****  

112 %* Updating historic variables %*
113 % hvar_n1(1:4) = eps_nlp;
114 hvar_n1(5)= r_n1 ;
115 hvar_n1(6)= q_n1 ;
116 %
*****  

117
118
119
120
121 %
*****  

122 %* Auxiliar variables
123 aux_var(1) = fload;
124 aux_var(2) = q_n1/r_n1;
125 aux_var(3) = (q_n1-H*r_n1)/r_n1^3;
126 aux_var(4) = c11_n1;
127 %
*****  

128

```

129
130
131
132
133
134
135
136
137
138
139

```

1 function hplot = dibujar_criterio_dano1(ce,nu,q,tipoc_linea,MDtype,n)
2 %*
*****  

3 %* PLOT DAMAGE SURFACE CRITERIUM: ISOTROPIC MODEL  

%*  

4 %*  

%*  

5 %* function [ce] = tensor_elastico (Eprop, ntype) %*  

6 %*  

%*  

7 %* INPUTS %*  

8 %*  

%*  

9 %* Eprop(4) vector de propiedades de material  

%*  

10 %* Eprop(1)= E----->modulo de Young  

%*  

11 %* Eprop(2)= nu----->modulo de Poisson  

%*  

12 %* Eprop(3)= H----->modulo de  

Softening/hard. %*  

13 %* Eprop(4)=sigma_u----->tensiõ final  

%*  

14 %* ntype %*  

15 %* ntype=1 plane stress  

%*  

16 %* ntype=2 plane strain  

%*  

17 %* ntype=3 3D  

%*  

18 %* ce(4,4) Constitutive elastic tensor (PLANE S.)  

%*  

19 %* ce(6,6) ( 3D)  

%*  

20 %*  

*****  

21  

22  

23 %*  

*****  

24 %* Inverse ce  

%*  

25 ce_inv=inv(ce);  

26 c11=ce_inv(1,1);  

27 c22=ce_inv(2,2);  

28 c12=ce_inv(1,2);  

29 c21=c12;  

30 c14=ce_inv(1,4);  

31 c24=ce_inv(2,4);  

32 %*  

*****  

33  

34  

35  

36

```

```

37
38
39
40 % ↵
*****
41 % POLAR COORDINATES
42 if MDtype==1 %Symmetric
43     tetha=[0:0.01:2*pi];
44     % ↵
*****
45     %* RADIUS
46     D=size(tetha);                      %* Range
47     m1=cos(tetha);                      %*
48     m2=sin(tetha);                      %*
49     Contador=D(1,2);                    %*
50     radio = zeros(1,Contador) ;
51     s1    = zeros(1,Contador) ;
52     s2    = zeros(1,Contador) ;
53
54     for i=1:Contador
55         radio(i)= q/sqrt([m1(i) m2(i) 0 nu*(m1(i)+m2(i))]*ce_inv*[m1(i) m2(i) 0 ↵
...
56             nu*(m1(i)+m2(i))]');
57
58         s1(i)=radio(i)*m1(i);
59         s2(i)=radio(i)*m2(i);
60
61     end
62     hplot =plot(s1,s2,tipos_linea);
63
64
65 elseif MDtype==2 %Tensile damage
66     tetha=[0,0:0.005:2*pi];
67     % ↵
*****
68     %* RADIUS
69     D=size(tetha);                      %* Range
70     m1=cos(tetha);                      %*
71     m2=sin(tetha);                      %*
72     Contador=D(1,2);                    %*
73     radio = zeros(1,Contador) ;
74     s1    = zeros(1,Contador) ;
75     s2    = zeros(1,Contador) ;
76     for i=1:Contador
77         radio(i)= q/sqrt([max(m1(i), 0) max(m2(i),0) 0 max(nu*(m1(i)+m2(i)),0)] ↵
*ce_inv*[m1(i) m2(i) 0 ...
78             nu*(m1(i)+m2(i))]');
79
80         s1(i)=radio(i)*m1(i);
81         s2(i)=radio(i)*m2(i);
82     end
83     hplot =plot(s1,s2,tipos_linea);
84
85
86 elseif MDtype==3 %Non-symmetric

```

```
87     tetha=[0:0.005:2*pi];
88     %*
*****  
89     %* RADIUS
90     D=size(tetha);                                %* Range
91     m1=cos(tetha);                                %*
92     m2=sin(tetha);                                %*
93     Contador=D(1,2);                                %*
94     radio = zeros(1,Contador) ;
95     s1    = zeros(1,Contador) ;
96     s2    = zeros(1,Contador) ;
97     for i=1:Contador
98         t=(max(m1(i),0)+max(m2(i),0)+max(nu*(m1(i)+m2(i)),0))/(abs(m1(i))+abs(m2(i))+abs(nu*(m1(i)+m2(i))));
99
100        radio(i)= q/(sqrt([m1(i) m2(i) 0 nu*(m1(i)+m2(i))]*ce_inv*[m1(i) m2(i) 0
...
101            nu*(m1(i)+m2(i))]')*(t+(1-t)/n));
102
103        s1(i)=radio(i)*m1(i);
104        s2(i)=radio(i)*m2(i);
105    end
106    hplot =plot(s1,s2,tipos_linea);
107
108
109
110 end
111 %*
*****  
112
113
114
115 %
*****  
116 return
117
118
119
120
```



```

51 % 1) sigma_v{itime}(icomp,jcomp) --> Component (icomp,jcomp) of the cauchy
52 % stress tensor at step "itime"
53 % REMARK: sigma_v is a type of
54 % variable called "cell array".
55 %
56 %
57 % 2) vartoplot{itime} --> Cell array containing variables one wishes ↵
to plot
58 %
59 % vartoplot{itime}(1) = Hardening variable (q)
60 % vartoplot{itime}(2) = Internal variable (r)%
61 %
62 %
63 % 3) LABELPLOT{ivar} --> Cell array with the label string for
64 % variables of "varplot"
65 %
66 % LABELPLOT{1} => 'hardening variable (q)'
67 % LABELPLOT{2} => 'internal variable'
68 %
69 %
70 % 4) TIME VECTOR - >
71 %
%%%%%%%%%%%%%%%
72
73 % SET LABEL OF "vartoplot" variables (it may be defined also outside this ↵
function)
74 %
75 LABELPLOT = {'hardening variable (q)', 'internal variable'};
76 LABELPLOT{3} = 'damage variable (d)';
77 LABELPLOT{4} = 'C11';
78
79 E = Eprop(1); nu = Eprop(2);
80 viscpr = Eprop(6);
81 sigma_u = Eprop(4);
82
83
84
85 if ntype == 1
86     menu('PLANE STRESS has not been implemented yet', 'STOP');
87     error('OPTION NOT AVAILABLE')
88     mstrain = 4;
89     mhyst = 6;
90 elseif ntype == 3
91     menu('3-DIMENSIONAL PROBLEM has not been implemented yet', 'STOP');
92     error('OPTION NOT AVAILABLE')
93 else
94     mstrain = 4;
95     mhyst = 6;
96 end
97
98 totalstep = sum(istep);
99
100
101 % INITIALIZING GLOBAL CELL ARRAYS

```

```

102 % -----
103 sigma_v = cell(totalstep+1,1) ;
104 TIMEVECTOR = zeros(totalstep+1,1) ;
105 delta_t = TimeTotal./istep/length(istep) ;
106
107
108 % Elastic constitutive tensor
109 % -----
110 [ce] = tensor_elasticol (Eprop, ntype);
111 % Init.
112 % -----
113 % Strain vector
114 % -----
115 eps_n1 = zeros(mstrain,1);
116 % Historic variables
117 % hvar_n(1:4) --> empty
118 % hvar_n(5) = q --> Hardening variable
119 % hvar_n(6) = r --> Internal variable
120 hvar_n = zeros(mhist,1) ;
121
122 % INITIALIZING (i = 1) !!!!*
123 % ****i*
124 i = 1 ;
125 r0 = sigma_u/sqrt(E);
126 hvar_n(5) = r0; % r_n
127 hvar_n(6) = r0; % q_n
128 eps_n1 = strain(i,:) ;
129 sigma_n1 = ce*eps_n1'; % Elastic
130 sigma_v{i} = [sigma_n1(1) sigma_n1(3) 0; sigma_n1(3) sigma_n1(2) 0 ; 0 0 sigma_n1(4)];
131
132 nplot = 3 ;
133 vartoplot = cell(1,totalstep+1) ;
134 vartoplot{i}(1) = hvar_n(6) ; % Hardening variable (q)
135 vartoplot{i}(2) = hvar_n(5) ; % Internal variable (r)
136 vartoplot{i}(3) = 1-hvar_n(6)/hvar_n(5) ; % Damage variable (d)
137 vartoplot{i}(4) = ce(1,1) ; % C11 (d)
138
139 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
140 %*****%
141 % INVISCID
142 % *****%
143
144 if viscpr == 0
145 for iload = 1:length(istep)
146     % Load states
147     for iloc = 1:istep(iload)
148         i = i + 1 ;
149         TIMEVECTOR(i) = TIMEVECTOR(i-1)+ delta_t(iload) ;
150         % Total strain at step "i"
151         % -----
152         eps_n1 = strain(i,:) ;
153         %*
154         %*      DAMAGE MODEL

```

```

155 % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % %
156 [sigma_n1,hvar_n,aux_var] = rmap_dano1(eps_n1,hvar_n,Eprop,ce,MDtype,n);
157 % PLOTTING DAMAGE SURFACE
158 if(aux_var(1)>0)
159     hplotSURF(i) = dibujar_criterio_dano1(ce, nu, hvar_n(6), 'r:',MDtype,n)
160 );
161     set(hplotSURF(i), 'Color',[0 0 1], 'LineWidth',1)
162 ;
163 end
164 %*****%
165 % GLOBAL VARIABLES
166 % *****
167 % Stress
168 % -----
169 m_sigma=[sigma_n1(1) sigma_n1(3) 0;sigma_n1(3) sigma_n1(2) 0 ; 0 0
sigma_n1(4)];
170 sigma_v{i} = m_sigma ;
171
172 % VARIABLES TO PLOT (set label on cell array LABELPLOT)
173 % -----
174 vartoplot{i}(1) = hvar_n(6); % Hardening variable (q)
175 vartoplot{i}(2) = hvar_n(5); % Internal variable (r)
176 vartoplot{i}(3) = 1-hvar_n(6)/hvar_n(5); % Damage variable (d)
177 vartoplot{i}(4) = aux_var(4); % C11 (d)
178
179 end
180 end
181 %*****%
182 %*****%
183 % VISCOSUS
184 % *****
185
186 else
187 for iload = 1:length(istep)
188 % Load states
189 for iloc = 1:istep(iload)
190 i = i + 1;
191 TIMEVECTOR(i) = TIMEVECTOR(i-1)+ delta_t(iload);
192 % Total strain at step "i"
193 % -----
194 timestep=TIMEVECTOR(i)-TIMEVECTOR(i-1);
195 eps_n = strain(i-1,:);
196 eps_n1 = strain(i,:);
197 % *
*****%
198 %* DAMAGE MODEL
199 % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % % %
200 [sigma_n1,hvar_n,aux_var] = rmap_dano2(eps_n,eps_n1,hvar_n,Eprop,ce,
MDtype,n,timestep);
201 % PLOTTING DAMAGE SURFACE
202 if(aux_var(1)>0)
203     hplotSURF(i) = dibujar_criterio_dano1(ce, nu, hvar_n(6), 'r:',MDtype,n)
204 );

```

```
204         set(hplotSURF(i), 'Color',[0 0 1], 'LineWidth',1) ↵
;
205     end
206
207 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
208 %*****GLOBAL VARIABLES*****
209 % Stress
210 % -----
211 %_sigma=[sigma_n1(1) sigma_n1(3) 0;sigma_n1(3) sigma_n1(2) 0 ; 0 0 ↵
sigma_n1(4)];
212         sigma_v{i} = _sigma ;
213
214
215 % VARIABLES TO PLOT (set label on cell array LABELPLOT)
216 % -----
217 vartoplot{i}(1) = hvar_n(6) ; % Hardening variable (q)
218 vartoplot{i}(2) = hvar_n(5) ; % Internal variable (r)
219 vartoplot{i}(3) = 1-hvar_n(6)/hvar_n(5) ; % Damage variable (d)
220 vartoplot{i}(4) = aux_var(4) ; % C11 (d)
221
222
223 end
224 end
225 end
226
```