COMPUTATIONAL MECHANICS TOOLS Course simulation project: Dynamics Analysis of a train wheel with Abaqus

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Outline

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- 2 Problem statement
- 3 Theoretical Framework
- 4 Methodology
 - Wheel geometry
 - Simulation setup
 - Boundary conditions
 - Mesh

5 Results

- Eigenfrequencies
- Eigenmodes
- Frequency of rotation coupling
- Sleeper contact frequency coupling
- Stick-slip transition wheel/rail
- 6 Conclusions
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Wheel squeal

- Acoustic pollution is one of the most common issues with rail transit in inhabited areas.
- One of the relevant sources of acoustic pollution is the so-called wheel squeal.

Wheel squeal is a high frequency, high pressure level sound caused by the vibration of the wheels that results in unacceptable noisy environments around the rail systems.

- Usually produced between 2 and 8 kHz.
- Characteristics of wheel squeal vary from vehicle to vehicle. It mainly depends on,
 - *Geometric factors*: wheel size and shape, curvature of rail, etc.
 - Environmental factors: temperature, humidity of air, etc.
 - Dynamic factors: linear velocity, angular velocity,...
- According to [3], there are up to 60 identified different parameters that can affect wheel squeal.

Problem statement

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Problem statement

- Analyze the dynamic response of a train wheel
- Squeal is generated between 2 and 8 kHz
- Study cases
 - Analyze if some modes of the wheel generate squeal.
 - Coupling between the wheel eigenfrequencies and wheel frequency due to rotation.
 - Coupling between position of sleepers and squeal phenomena.

L Theoretical Framework

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L Theoretical Framework

The equation of motion is,

Free undamped system

$$M\ddot{u} + Ku = 0$$

where, in general (multidegree-of-freedom system)

- M is the so-called mass matrix
- K is the stiffness matrix of the system
- **u** is the displacement vector

• Solution of this equation can be found by assuming a solution of the form

$$\boldsymbol{u}(t) = \boldsymbol{a}\phi(t) \tag{2}$$

where \boldsymbol{a} is a vector of constant parameters and $\phi(t)$ is just a function of time.

• The configuration of the system, given by the vector

$$egin{array}{l} a = egin{cases} a_1 \ a_2 \ dots \ a_n \end{pmatrix} \end{array}$$

is known as the *mode shapes*.

- Solution procedure $\boldsymbol{u}(t) = \boldsymbol{a}\phi(t) \Rightarrow \boldsymbol{\ddot{u}} = \boldsymbol{a}\ddot{\phi}(t)$
- Plug this into the former equation, rearrange and after some algebra, it yields

$$-\omega^2 M a + K a = 0 \Rightarrow K a = \omega^2 M a \Rightarrow M^{-1} K a = \omega^2 a$$

and this is an eigenvalue problem

Eigenvalue problem

$$\boldsymbol{D}\boldsymbol{a} = \omega^2 \boldsymbol{a} \Rightarrow det(\boldsymbol{D} - \omega^2 \boldsymbol{I}) = 0$$

(3)

where $D = M^{-1}K$ is the so-called *dynamical matrix* and I is the identity matrix of the required order [5].

L Theoretical Framework

- By finding the solution for this problem, we obtain as many couples ω, a as degrees of freedom of the system.
- ω_i are the eigenvalues or *natural frequencies*.
- a_i are the eigenvectors or mode shapes.
- This information could be used to determine if an excitation is close to one of the natural frequencies what could cause the so-called resonance phenomena.

L_Methodology

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• Wheel data (geometry and materials)



Width	t	[m]	0.05
Internal diameter	d	[m]	0.10
External diameter	D	[m]	1.00
Density	ρ	$[Kg/m^3]$	7800
Yong Modulus	E	[Pa]	210E9
Poisson Ratio	u	[-]	0.25

Figure 1: Geometry and material data for the train wheel.

- Wheel is sketched using the Abaqus CAD mode.Sketch the 2D model (two concentric circles) and then extrude.
- Create the section and assign the material. In this case, linear elastic behavior is assumed.



Figure 2: Train wheel CAD model.

- Create a step and set the procedure to "Linear perturbation" and select "Frequency".
- Select value and introduce the desired number of eigenvalues (frequencies), 10

🜩 Edit Step	×		
Name: NaturalFreq			
Type: Frequency			
Basic Other			
Description: 10 first natural freqs			
Nlgeom: Off 🤌			
Eigensolver: Lanczos Subspace AMS			
Number of eigenvalues requested: O All in frequency range			
● Value: 10			
Frequency shift (cycles/time)**2:			
Minimum frequency of interest (cycles/time):			
Maximum frequency of interest (cycles/time):			
✓ Include acoustic-structural coupling where applicable			
Block size: O Default Value:			
Maximum number of block Lanczos steps: Default Value: 			
Use SIM-based linear dynamics procedures			
Include residual modes			

Figure 3: Setup for the eigenvalue problem.

L_Methodology

Boundary conditions

- Assign boundary conditions for the dynamic analysis
 - Prescribe displacement of nodes in the hole \Rightarrow encastre
 - Prescribe displacement of nodes of line AB \Rightarrow X-symmetry



Figure 4: Representation of the boundary conditions

- Wheel is discretized with hexahedra finite elements.
- Use approximate global size equal to 0.05.



Figure 5: Mesh with hexahedra elements Magdalena Pérez Lanfranco Samuel Parada Bustelo ABAQUS SIMULATION PROJECT

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Results

L_Eigenfrequencies

• Eigenfrequencies of the wheel are collected in Table 20,

Mode	Frequency $[Hz]$
1	24.759
2	25.116
3	26.256
4	38.749
5	48.386
6	82.899
7	87.851
8	133.11
9	141.63
10	146.99

Table 1: Wheel's natural frequencies

L_Results

L_Eigenmodes

• In the next figures, we show the eigenmodes. Original shape is also included for comparison.



Figure 6: Mode 1

Results

L_Eigenmodes



Figure 7: Mode 2

Results

L_{Eigenmodes}



Figure 8: Mode 3

Results

L_{Eigenmodes}



Figure 9: Mode 4

Results

L_Eigenmodes



Figure 10: Mode 5

Results

L_Eigenmodes



Figure 11: Mode 6

Results

L_Eigenmodes



Figure 12: Mode 7

Results

L_Eigenmodes



Figure 13: Mode 8

Results

L_{Eigenmodes}



Figure 14: Mode 9

Results

L_{Eigenmodes}



Figure 15: Mode 10

L_Results

Frequency of rotation coupling

- Study the possible coupling between natural frequencies and frequency of rotation when the train travels at $v_{max} = 350 \ km/h = 97.22 \ m/s$
- Calculate angular velocity

$$\omega_{max} = \frac{v_{max}}{R} = \frac{97.22 \ m/s}{0.5m} = 194.44 \ rad/s$$

Angular velocity

$$\omega_{max} = 194.44 \ \frac{rad}{s} \cdot \frac{1 \ rev}{2\pi \ rad} = 30.946 \ rev/s \ [Hz] \tag{4}$$

L_Results

Frequency of rotation coupling

Mode	Frequency $[Hz]$
1	24.759
2	25.116
3	26.256
4	38.749
5	48.386
6	82.899
7	87.851
8	133.11
9	141.63
10	146.99

- ω_{max} is close to the third mode frequency \Rightarrow resonance may appear.
- Wheel will be suffering severe deformations over time.
- For high enough values of amplitude, wheel can enter into stick-slip transition ⇒ squeal

└─Sleeper contact frequency coupling

- Analyze the possible coupling between the sleepers and the wheel.
- Sleepers are the transverse beams holding the train rails located every 60 cm in this case.
- Assume a linear velocity v for the train. Thus, the frequency at which the train will pass by a sleeper is,

Contact frequency with sleepers $v \frac{m}{s} \cdot \frac{1 \ cycle}{0.6 \ m} = f_c \ \frac{cycle}{s} [Hz] \tag{5}$

Results

Sleeper contact frequency coupling

Mode	Frequency $[Hz]$	Velocity of coupling $[m/s]$
1	24.759	14.85
2	25.116	15.06
3	26.256	15.75
4	38.749	23.24
5	48.386	29.02
6	82.899	49.73
7	87.851	52.71
8	133.11	79.86
9	141.63	84.97
10	146.99	88.19

Table 2: Traveling speeds that cause coupling

L_Results

Sleeper contact frequency coupling

- If the frequency of contact f_c is equal to any of the natural frequencies \Rightarrow resonance \Rightarrow vibration of the wheel will be amplified and the stick-slip transition phenomenon will appear.
- Coupling seems to be specially relevant for low speeds ⇒ consider the case when the train is entering or leaving a station.

L_Results

└─Stick-slip transition wheel/rail

The stick-slip phenomenon is a type of spontaneous motion that can occur while two objects are sliding over each other

- Two surfaces alternating between two states: sticking to each other and sliding over each other.
- If a force large enough is applied to one of the surfaces, it will start sliding and friction coefficient decreases from μ_s to μ_d.
- When it happens between wheel/rail surfaces, the wheel can oscillate and radiate the squeal noise [1].

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Stick-slip transition wheel/rail	

- Squeal can be also generated when the train passes through a curved section or a switch between rails.
- During curve passages wheels suffer lateral creepage as they are not perfectly aligned.
- The rolling angle, α, is the angle between the rolling direction and the direction of the movement.

Lateral creepage

The lateral creepage is defined as the tangent of the rolling angle

$$LC = \tan \alpha$$

(6)

Conclusions

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- Wheel squeal is still a complicated issue with varied causes [2]: geometric, atmospheric, material-related, etc.
- More research is needed to fully understand this phenomena and find reliable solutions.
- Solutions? Change location of sleepers to an arbitrary one; lubrication stations at critical points...

To completely eradicate wheel squeal?

MAGLEV TRAIN \Rightarrow no wheel vibration

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