FLOOD RISK IN CASE OF YESA'S DAM BREAK





Lorenzo Gracia Llinares

CIMNE / Universidad Politécnica de Cataluña

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Motivation



Tous (1982) and Vajont (1963)

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- 1. Introduction and Matemathical Foundations
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Incompressible Navier Stokes 3D for Isotropic Newtonian fluids

$$\partial_t \mathbf{u} + (\mathbf{u} \cdot \nabla)\mathbf{u} - \nu \Delta \mathbf{u} + \nabla p = \mathbf{f}$$

$$abla \cdot \mathbf{u} = \mathbf{0}$$

- Kolmogorov Theory (1941)
 - It allows to obtain estimations of the scales necessary for the discretization of the problem

Example of Kolmogorov Theory (1941)

$$u = \frac{l_0}{Re^{3/4}} \qquad \tau = \frac{\tau_0}{Re^{1/2}}$$

where l_0 is the characteristhic length, ν is the smallest space scale, Re is the Reynolds Number, τ_0 is the charactheristic time and, τ is the smallest time scale

• Using $l_0=1$ m and $\tau_0=1$ seg, finally we obtain;

$$N = Re^{11/4}$$

For a hydraulic problem, an usual value for the Reynolds number can be of order to 10^6 then the needed number of nodes would be 10^{16}

- Simplifications of Navier Stokes Equations
 - $\,\circ\,$ Study of turbulent flux \Rightarrow Application of Reynold's Theory

$$u = \overline{u} + u'$$

where \overline{u} is the average variable and u' is the turbulent fluctuation.

$$\overline{u} = \frac{1}{t_2 - t_1} \int_{t_1}^{t_2} u dt$$

Depth integration

$$u=\frac{1}{h}\int_{z_0}^{z_0+h}\overline{u}dz$$

Saint Venant 2D

- Neglecting Coriolis effect (not important in rivers)
- $\circ~$ Applying Leibnitz rule derivation under the integral sign
- Finally we obtain

$$\frac{\partial h}{\partial t} + \frac{\partial (hu)}{\partial x} + \frac{\partial (hv)}{\partial y} = 0$$
$$\frac{\partial (hu)}{\partial t} + \frac{\partial}{\partial x} (hu^2 + g\frac{h^2}{2}) + \frac{\partial (huv)}{\partial y} = gh(S_{0x} - S_{fx})$$
$$\frac{\partial (hv)}{\partial t} + \frac{\partial (huv)}{\partial y} + \frac{\partial}{\partial y} (hv^2 + g\frac{h^2}{2}) = gh(S_{0y} - S_{fy})$$

2. Software IBER

- 2D Dimensinal Analysis through Saint Venant 2D
- Finite Volumes in 2D
- GID Interface
- Non-linear Hyperbolic System \Rightarrow Roe Scheme



- Yesa's Dam and Reservoir
 - Gravity dam (480.000 m^3 of concrete)
 - Crest length: 398 m
 - Capacity: 446.90 hm³
 - Area: 2098 ha
 - Area of basin: 2170 Km²



Ubication of Yesa's Dam

Input Data

- MDT 25x25 (ASCII format)
- A file of land use (SIOSE 2005)
- Characteristhic curve of the reservoir



Topographic map of study area

- Mesh and Roughness
 - A structured triangular mesh
 - $\circ~$ Size element: 200
 - Number of elements: about 1.000.000



Manning map

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- Break according ICOLD
 - Duration: 24 hours
 - \circ Partially breach, 1/3 of the whole body
 - Time of breakage: 900 seg

4. Results

• Maximum drafts



4. Results

• Sangüesa's drafts





4. Results

• Evolution in time of Sangüesa's drafts



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5. Conclusions

- Critical situation for Sangüesa's village in case of break, necessity of an evacuation plan for the population
- Some phenomena are not taken into account since we are using Saint Venant 2D, but in the case of this study, for instance, turbulence can be neglected
- Related with the simulation, this software provides accurate results but the computational cost for large areas of study are extremly high
- The obtained results are in consonance with the developed studies some years ago by Dr. Antonio Casas (*University of Zaragoza*)

THANK YOU FOR YOUR ATTENTION!

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